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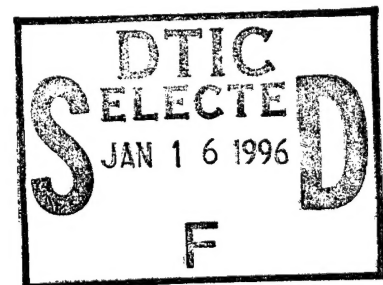
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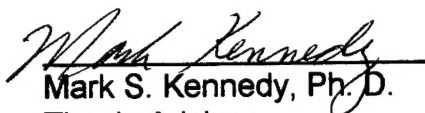
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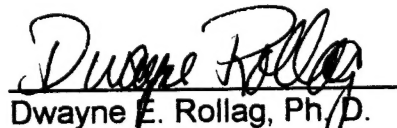
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## Modeling the Fate and Transport of TNT in Soils

This thesis is approved as a creditable and independent investigation by a candidate for the Master of Science degree and is acceptable for the meeting the thesis requirements for this degree. Acceptance of this thesis does not imply that the conclusions reached by the candidate are necessarily the conclusions of the major department.

  
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## ABSTRACT

### Modeling the Fate and Transport of TNT in Soils

Jeffrey C. Gillen

June 5, 1995

The model, BIOROOT, was implemented as a predictive tool to assess the fate and transport and to determine the effects of vegetative remediation anticipated during remediation of trinitrotoluene (TNT) contaminated soils. The model is designed to incorporate biological, physical, chemical, and environmental factors in predicting the degradation fate of trinitrotoluene (TNT). Lagoons from an explosives washout facility at the Umatilla Depot Activity near the city of Hermiston, Oregon were utilized to illustrate the model. Four scenarios were simulated: 1). no degradation of the TNT contaminant, 2). degradation half life values of 1 year, 3). amending the soil with 10% organic material, and 4). initiating vegetative remediation using the alfalfa plant. The amount of contaminant leached from the upper soil matrix after 1300 days was 7300 g, 1400 g, 18 g, and -50 g TNT respectively. Vegetative remediation demonstrated an ability to prevent TNT from entering the soil-water phase and leaching into the ground water. Vegetation was also capable of capturing and remediating contaminant not in direct contact with the root system.

**Key words:** remediation, vegetation, model, TNT, munitions, wastes.

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## **CHAPTER 1.**

### **INTRODUCTION**

Today, there are numerous hazardous waste sites in almost every state that are contaminated from explosive compounds. The U.S. Army has been charged with initiating and overseeing a large research and development program focused on finding remediation solutions to the environmental problems caused from munitions manufacture, maintenance, and disposal operations. The predominant problem exists at former army ammunition plants operated during the past century. The total quantity of contaminated soil at these ammunition plants has been estimated to approach 1 billion tons (Majors et al. 1994). As of 1986, there were only six ammunition plants that manufacture or conduct load, assembly, and packing operations with explosive compounds such as trinitrotoluene (TNT). These plants produced 1,900,000 pounds of TNT monthly. Maximum production capabilities were conservatively estimated to be at least 15 times the current production level (Roberts, 1986). During the past century, the U.S. Army estimates that approximately one billion tons of soil are contaminated from explosive compounds. The contamination at ammunition plants exists at concentrations averaging less than 200 ppm (Majors et al. 1994).

### ***SCOPE OF THE PROBLEM***

Three major industries are affected by explosive wastes: the military,



munitions manufacturing, and mining. The military is significantly impacted due to its diverse applications of explosives and munitions. Operational activities such as weapons maintenance and disposal produce the majority of the contamination problems. Almost every military installation has a weapon storage area where routine maintenance and disposal activities are performed.

Maintenance operations often produce waste streams known as "pink waters" due to its characteristic color. Pink waters are wastewaters generated during loading, packing, handling, and disposal operations. For instance, disposal operations may use hot water to remove the explosive from the bomb / shell casing. The mixture of disposed explosive in the wash water turns a pinkish hue when exposed to light. Historically, disposal activities placed unserviceable units into a dedicated trench and were remotely detonated. This trench, commonly known as a burn pit, was often nothing more than an open ditch located on a remote section of the base.

Manufacturers, including the pyrotechnics and fireworks industries, are primarily impacted from the effluent created during the production and purification of explosives. The purification of TNT generates a waste stream known as "red water" due to its characteristic color resulting from sulfite reactions with the explosive impurities. Finally, the mining industry is impacted from explosive residues leaching into the soil and ground water from waste heap piles and abandoned mines.

The explosive compounds of primary interest are 2,4,6-trinitrotoluene (TNT), Royal Demolition Explosive (RDX) hexahydro-1,3,5-trinitro-1,3,5-triazine, and High Melting Explosive (HMX) octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine. Of the three, TNT contamination is the most prevalent due to its extensive use and manufacture during the past century. Related explosive precursors and daughter compounds include dinitrotoluene (DNT), trinitrobenzene (TNB), dinitrobenzene (DNB), and many other nitroaromatic and aliphatic compounds. These are used to manufacture not only explosives but also pharmaceuticals, pesticides, polyurethanes, foams, dyes, pigments, coatings, elastomers, and waterproofing agents (Roberts et al. 1986, Majors et al. 1994, Gorontzy et al. 1994)

#### ***POTENTIAL FOR DEGRADATION***

Nitroaromatic compounds are xenobiotic (man-made) and highly recalcitrant. Xenobiotic compounds are not naturally occurring in the environment and therefore tend to resist natural decomposition processes. This makes them very difficult to remediate when they are released into the environment. Many of the nitroaromatic compounds and their daughter products exhibit toxic and mutagenic effects on life forms such as bacteria, fungi, yeast, unicellular algae, copepods, and oyster larvae (Won et al. 1974 and Nay et al. as reported by Marvin-Sikkema, 1994). Researchers have had difficulty demonstrating complete mineralization of explosives to carbon dioxide and water

under aerobic environments, or methane under anaerobic conditions.

TNT degradation has been shown to occur through two primary pathways. One, oxidation of the methyl group to form trinitrobenzene which can be degraded by sunlight, ozonation, and catalysis with the soil particles. Two, reduction of the nitro groups to form hydroxyamino and amino intermediates. Of the two pathways, the latter has been the observed preferential sequence (Majors et al. 1994, McCormick et al. 1976).

#### **RESEARCH OBJECTIVES**

The objective of this research was to implement a model that can be utilized as a predictive tool by environmental engineering professionals to assess the likely fate and transport of explosive compounds in the environment and to assist them in determining remediation alternatives for that particular site. The model incorporates physical, chemical, and environmental factors that directly affect the compound's rate of degradation and transport in the environment .

For the purposes of this thesis, a U.S. Army site known as the Umatilla Depot Activity (UMDA), near Hermiston, Oregon was used to illustrate the proposed model. The site of specific interest within the Depot was an explosives washout facility utilized to demilitarize conventional ordinance. The operation utilized a pressurized hot water system to extract (washout) the explosives from the bomb and shell casings. Wastewater from the washout facility was

impounded into an unlined lagoon system that allowed unrestricted percolation into the underlying soil, and ground water, and volatilization into the atmosphere (MKES et al. 1992).

## CHAPTER 2.

### LITERATURE REVIEW

To further understand the complexity of the problem, a brief discussion of how these compounds are manufactured and the prevailing chemical reaction mechanisms may provide insight as to why these compounds are so resistant to natural environmental degradation processes. A review of the available research and literature summarizes the controlling degradation systems for explosive compounds such as TNT, RDX, and HMX. Figure 2-1 illustrates the chemical structures of these three chemical compounds. To date, none of the cited research has been able to establish or determine degradation pathways of nitroaromatic compounds to complete mineralization. However, the research has identified some very important and critical partial degradation pathways of these very recalcitrant, xenobiotic compounds.

#### ***TNT MANUFACTURE***

Trinitrotoluene (TNT) is the common name for 2,4,6-trinitrotoluene. TNT is formed when toluene is successively reacted with nitric acid ( $\text{HNO}_3$ ) in the presence of sulfuric acid ( $\text{H}_2\text{SO}_4$ ). Stoichiometrically, toluene releases hydrogen ( $\text{H}^+$ ) ions from its ring as the nitric acid releases hydroxide ( $\text{OH}^-$ ) ions, thus allowing the nitro group(s) to attach to the unbalanced (charged) site on the ring structure. The nitration reaction of toluene to form trinitrotoluene requires 1 mole

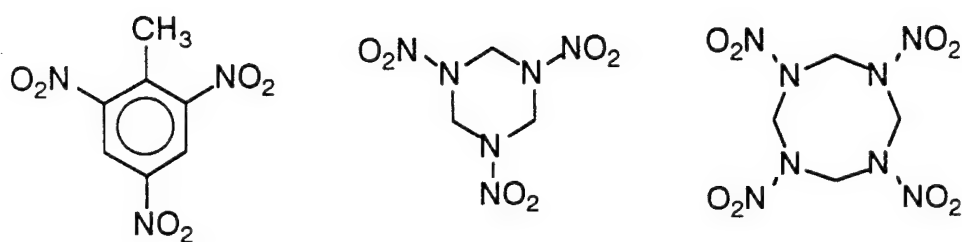


Figure 2-1. Chemical Structure of TNT, RDX, & HMX.

of trinitrotoluene to react with 3 moles of nitric acid to produce 1 mole of TNT and 3 moles of water. Figure 2-2 describes the chemical equation reaction.

Toluene, which is a single methyl ( $\text{CH}_3$ ) group attached to a benzene ring, is classified as an ortho-para directing group (Linstromberg et al. 1983). This means that during the addition of the first nitro group to the toluene ring there is a 70% preferential attachment at the *para* position rather than the *ortho* position. After the first nitro ( $\text{NO}_2$ ) group is attached, the  $\text{NO}_2$  group, which is a strong *meta* director, will dominate subsequent reaction mechanisms by placing the additional  $\text{NO}_2$  groups *meta* to the original  $\text{NO}_2$  group. Thus, successive nitration of the toluene ring directs the initial  $\text{NO}_2$  group to the *para* position and the additional  $\text{NO}_2$  groups *meta* from the  $\text{NO}_2$  group. Successive nitration of the first two  $\text{NO}_2$  groups is relatively straight forward. However, the addition of the third  $\text{NO}_2$  group at the 6- position is more difficult because the two existing  $\text{NO}_2$  groups have significantly reduced the overall activity of the compound.

This nitration reaction is 95% efficient in producing 2,4,6-TNT ( $\alpha$ -TNT). The remaining 5% produces other unsymmetrical TNT isomers (Hao et al. 1991) such as 2,4,5-TNT or trinitrobenzene (TNB). Raw TNT must be purified to separate the impurities from the  $\alpha$ -TNT. This is done by reacting the raw TNT with sulfite. The impurities react with the sulfite to produce sulfonated compounds that allow the  $\alpha$ -TNT to be easily stripped away. The resulting sulfonated waste stream has a characteristic reddish color and is known as "red water."

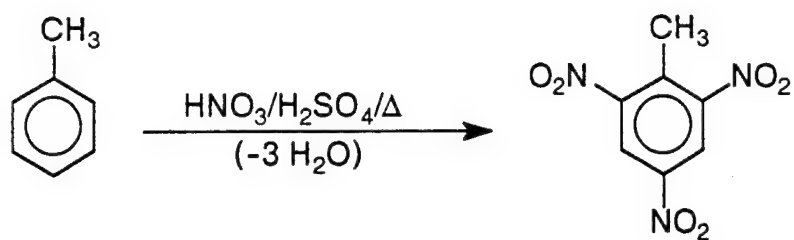


Figure 2-2. Reaction Mechanism for the Production of TNT from Toluene.



## **TOXICOLOGY AND HEALTH EFFECTS**

Compounds exist naturally in the environment in which we live. When these compounds adversely impact any species of life or cause an imbalance in the ecological stasis of the indigenous life forms, the compound is considered to be toxic to that environment. Toxic compounds may quickly disrupt the entire life cycle within that particular ecosystem or cause regional or global impacts. Thus understanding the toxic characteristics of individual and conglomerate compounds will help prevent negative insults to the environment, and assist in the restoration of negatively impacted ecological systems.

### **Toxicology.**

Won et al. (1976) conducted mutagenic and toxicological studies on TNT and its intermediate metabolites. Won determined that TNT was very toxic to green alga, oyster larvae, and tidepool copepods and mutagenic to *salmonella typhimurium*. The initial reductive metabolites did not exhibit acute toxicity nor mutagenicity to the test populations.

Phillips et al. (1993) conducted soil toxicity studies using the earthworm as the test species. Three different ammunition plants provided various soil types, contamination levels, and contamination sources. Earthworms were hardier than Phillips' research team had anticipated. The worms gained weight in half the tests and survived all but one of the tests. Similar results were observed for the

RDX and HMX treatments. One test involving forest soils exhibited lethal effects at concentrations of 150  $\mu\text{g/g}$ . Earthworms were able to thrive in all of the other soils even at higher TNT concentrations (maximum of 500  $\mu\text{g/g}$ ), but the forest soil exhibited inhibitory characteristics on the worms above the 150  $\mu\text{g/g}$  concentration. Philips offers that other soil constituents such as increased organic content and soil pH may contribute to this peculiar observation. The difference in organic content in the forest soils (5.9%) could be a primary factor over the other test soils organic content (1.4%).

#### *Mammalian Toxicology*

Shugart et al. (1991) conducted research at the Alabama ammunition plant to determine whether indigenous wildlife (deer, rabbits, and quail) were bioaccumulating explosive contaminants from ingesting surrounding water, soil, and plant life. Shugart referenced El-Hawari (1981) for determining the metabolites excreted from laboratory animals injected with TNT. Tissue samples were collected and did not indicate any TNT compound above 0.2 ppm nor was there any observed adverse affect on the wildlife. This led to the conclusion that the impacts on the wildlife would be minimal.

Roberts (1986) cites numerous researchers results. Specifically, laboratory animals have provided critical data not only in establishing their specific species response to acute doses of TNT but the data is also correlated to infer potential human response factors.

## Health Effects.

Explosive compounds are one of the few industrial compounds that are well documented in terms of human response factors. This comes from the unfortunate exposures that were incurred during manufacturing operations. Civilian and military munitions workers were exposed to compounds such as TNT, DNT, TNB, DNB, toluene, benzene, and other explosive precursors.

Roberts et al. (1986) compiled a comprehensive data summary on trinitrotoluene which summarizes significant research and reviews. Specifically, Roberts' report is comprehensive with detailed sections on toxicology, health effects and an extensive reference bibliography.

TNT has been shown to cause numerous effects on the liver, kidneys, heart, blood, pancreas, and central nervous system. Minor to moderate exposures result in significant hematological changes such as decreased blood counts in hemoglobin, red blood cells (RBC), and platelets; Heinz body formations; RBC dyscrasias; white blood cells changes (lymphocytosis and leukocytosis); and capillary fragility (causing nosebleeds and skin or membrane hemorrhages). Exposures at high concentrations may cause cyanosis or methemoglobinemia (RBC anemia). Chronic exposures in munitions (TNT) workers have experienced hemolytic anemia, cardiac effects such as dull heart beats, murmurs, EKG abnormalities, neurotoxicity, pancreatic toxicity, and nephrotoxicity (kidneys) which increases filtration rates and urination frequency.

Severe TNT exposures have caused death after the onset of acute effects including: yellow atrophy of the liver, aplastic anemia, bone marrow hypoplasia, and hepatotoxicity of the blood. The list of ailments is quite lengthy. Listing the above health conditions demonstrates the effects that TNT exposure has on the various organs and tissues of the human body.

Roberts cites a few researchers', Jaffe et al. (1973), Rosenblatt et al. (1980), and Zakhari et al. (1978), reviews of acute exposure studies conducted on human "volunteers" during the 1940s. Exposure routes varied from oral, dermal (hands), and respiratory pathways. Past human "volunteer" and munitions workers documented health effects over a 60 year period (1917 through 1976) and provided invaluable data on human physiological responses to exposures from munitions compounds. Occupational exposure routes were generally from airborne vapors and dusts. Personnel normally exposed include munitions manufacturing personnel, munitions maintenance personnel, tunnelers, and miners.

Roberts' report (1986) indicates teratogenic (reproductive) effects have been reported (by Jaffe et al. 1973) to cause symptoms of irregular menstruation in female munitions workers resulting from chronic TNT intoxication. Male reproductive responses may be inferred from rat studies where testicular atrophy was questionably observed (by Dilley et al. 1978).

The data from human and animal exposures are critical factors in

establishing occupational and public health standards. Animal studies provide extrapolative evidence in determining lethal concentrations ( $LC_{50}$ ) and lethal dosages ( $LD_{50}$ ) of compounds such as TNT and other explosives. These standards are designed to minimize adverse effects to the public from chronic low dose exposures. Specifically, the EPA has adopted a protection scheme to assess whether "ambient" exposures are capable of causing at least one additional case of cancer in a population of one million people (1:1,000,000). These assessments can take the form of regulatory compliance (law) or strongly encouraged Health Advisories. The Department of Labor's Occupational Safety and Health Administration (OSHA) established occupational threshold limit values (TLVs) and maximum permissible exposure limits (PELs). TLVs provide regulatory guidelines on the maximum amount of contaminant that an individual can be safely exposed to without adverse health effects. The American Conference of Governmental Industrial Hygienists (ACGIH 1995) established TLVs of 0.5 ppm for TNT and 0.15 ppm for DNT. Both chemicals are annotated as being suspected human carcinogens. TLVs do not suggest that employers intentionally expose employees to chemical (or physical) hazards. The use of engineering controls, personal protective equipment, and chemical substitution are effective tools that employers are highly encouraged to utilize in order to minimize work related injuries and illnesses.

### *Health Advisories*

In 1991, Roberts et al. established EPA Drinking Water Health Advisories (HA) for environmental contaminants specific to the U.S. Army. The EPA and U.S. Army entered into a memorandum of understanding to develop drinking water health advisories. An important aspect of health advisories are that they are not legally binding contamination levels even though they may be respected as such. Health advisories are calculated in a three step process by: a) determining the highest reference dose (RfD) which will not cause harmful health effects, b) establishing the drinking water exposure level (DWEL), and c) calculating the lifetime health advisory. Health advisories account for adult lifetime exposures, and one or ten day exposures for children. A child weighing 10 kilograms is assumed to drink 1 liter of water per day, while the average adult weighs 70 kg and consumes 2 liters of water per day. The reference dose is based on the maximum allowable concentration in which there is No Observable Adverse Effect Level (NOAEL) or the Lowest Observed Adverse Effect Level (LOAEL). The HA concentrations of four munitions compounds from Roberts' report are summarized in Table 2-1.

Explosive compounds are toxic to a wide variety of biological life forms that have been associated with traditional in situ remediation operations. Xenobiotic contaminants either impair the microbe or the microbes cannot consume the contaminant as a carbon source.

Table 2-1. Drinking Water  
Health Advisories  
(Roberts et. al. 1991)

Criteria	Concentration (mg/l)			
	TNT	DNB	RDX	HMX
1 Day HA	0.02	0.04	0.10	5.00
10 Day HA	0.02	0.04	0.10	5.00
Long Term HA				
Child	0.02	0.04	0.10	5.00
Adult	0.002	0.14	0.40	20.00
Lifetime HA	0.002	0.001	0.002	0.40
DWEL	0.02	0.005	0.10	2.00
EPA Cancer Group	C	D	C	D
NOAEL (mg/kg/day)		0.4	0.3	50
LOAEL (mg/kg/day)	0.5 (dogs)	1.14 (rats)	1.5 (rats)	115 (rats)
Uncertainty Factor	2		1	

The quest by the majority of the researchers has been to identify specific organism(s) that may be responsible for or capable of degrading the target compound. The focus of late has been centered around fungal systems and highly enriched cultures, identified from natural systems, that are capable of metabolizing the contaminant. Higher life orders, specifically mammals, have an ability to metabolize or excrete the contaminant. Mammals are not utilized as a viable remediation process.

#### ***DEGRADATION PATHWAYS***

Determining the degradation reactions from laboratory research studies is the first step to understanding how the same reaction processes can be implemented under actual field conditions. Laboratory research provides degradation kinetics under controlled conditions that can be extrapolated to estimate the controlling parameters that affect full scale remediation. Modeling provides a predictive tool that can be used to evaluate, correlate, and calibrate the predictive parameters derived from the laboratory studies to full scale, field remediation processes. The following researchers have conducted critical laboratory research in their quest to degrade explosive compounds.

McCormick et al. (1976) first postulated that one of two reaction pathways may occur during the degradation of TNT: reduction of the  $\text{NO}_2$  groups or oxidation of the methyl group. In the last ten years, the majority of the research has been to establish the degradation pathways of nitroaromatic compounds via



complete mineralization either aerobically or anaerobically producing carbon dioxide and water, or methane, respectively. Unfortunately, mineralization reactions have been difficult to determine and document.

#### Methyl Oxidation Pathway

Oxidation of the methyl ( $\text{CH}_3$ ) group involves the sequential transformation to an alcohol ( $\text{CH}_2\text{OH}$ ), aldehyde ( $\text{CHO}$ ), carboxylic acid ( $\text{COOH}$ ), and finally releasing  $\text{CO}_2$  from the nitroaromatic ring. Trinitrobenzene is formed if the carboxylic acid group leaves the ring as carbon dioxide (Majors et al. 1994). Spanggord's (et al. 1980) study supported this reaction pathway because concentrations of trinitrobenzaldehyde, trinitrobenzoic acid, and TNB were observed during the study. Aerobic conditions in the top few inches of soil provide a desirable environment for methyl oxidation to take place. Figure 2-3 illustrates the oxidation of the methyl group through various transformation products.

#### Nitro Reduction Pathway

The majority of the research has focused on the reduction of the  $\text{NO}_2$  groups. Additionally,  $\text{NO}_2$  transformation products have been observed more often in natural environments than the methyl intermediates.  $\text{NO}_2$  reduction involves the successive transformation of each  $\text{NO}_2$  group to a hydroxylamino ( $\text{NHOH}$ ) group and then to an amino ( $\text{NH}_2$ ) group before the next  $\text{NO}_2$  group is

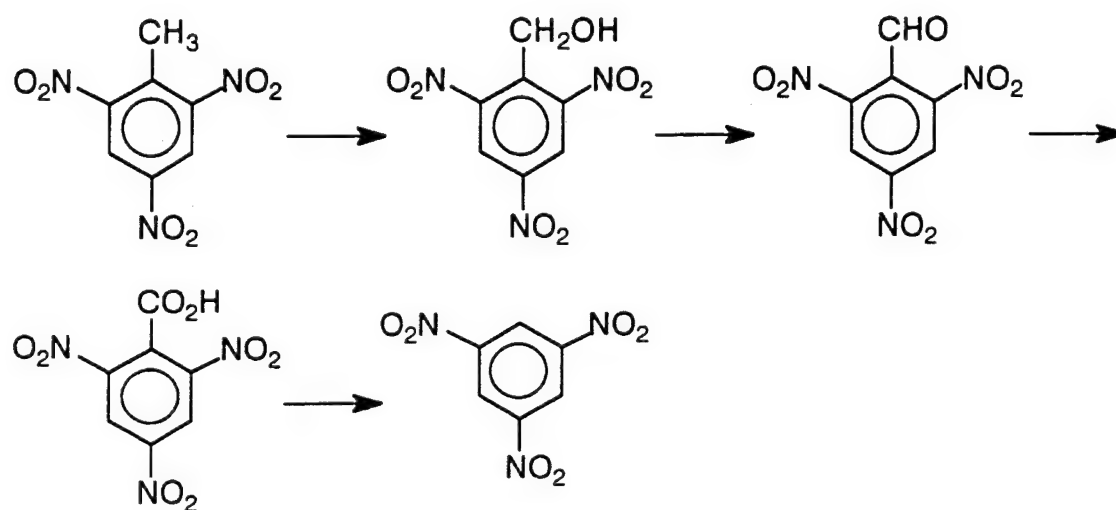


Figure 2-3. Oxidation of TNT's Methyl Group.

reduced. Once all three  $\text{NO}_2$  groups are converted, triaminotoluene (TAT) is formed. Triaminotoluene is very unstable and has been very difficult to measure analytically in the laboratory.

Reduction of  $\text{NO}_2$  may also involve the dimerization of adjacent intermediately reduced TNT molecules to form azoxy-toluenes such as 2,2',4,4'-tetrinitro-6,6'azoxytoluene or 2,2',6,6'-tetrinitro-4,4'azoxytoluene (Won et al. 1974, Majors et al. 1994). This secondary pathway is also shown in Figure 2-4. The production of these dimers is more pronounced under aerobic environmental conditions. Researchers that observed the azoxy compounds noted no further degradation of them. Therefore, the production of azoxy intermediates is undesirable and should be minimized or altogether prevented.

The degradation of TNT via the  $\text{NO}_2$  reduction pathway is preferred over the methylation or incomplete reductions that produce very recalcitrant dimers. Controlling the oxygen conditions is crucial to forcing the reaction sequence specific to the needs of the hazardous waste site. Soils near the water table are very low in free available oxygen, therefore, they tend to behave in an anaerobic fashion.

The production of the azoxy dimers can be attributed to whether aerobic conditions were encountered after initial anaerobic degradation conditions began. Inducing anaerobic treatments should be cost effective as lower volumes of materials are required to maintain an anaerobic versus aerobic environment.

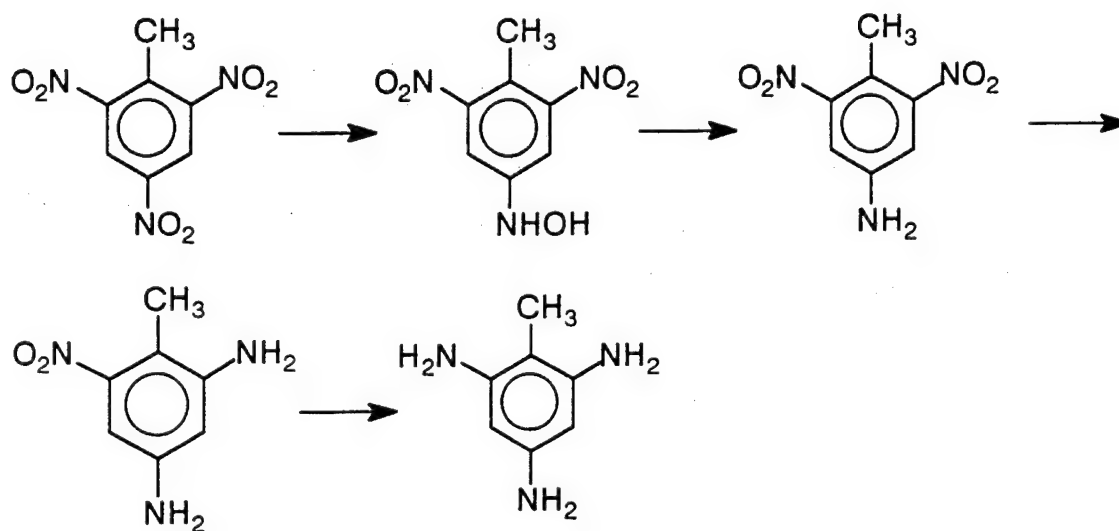


Figure 2-4A. Successive Reduction of TNT's Nitro Group.

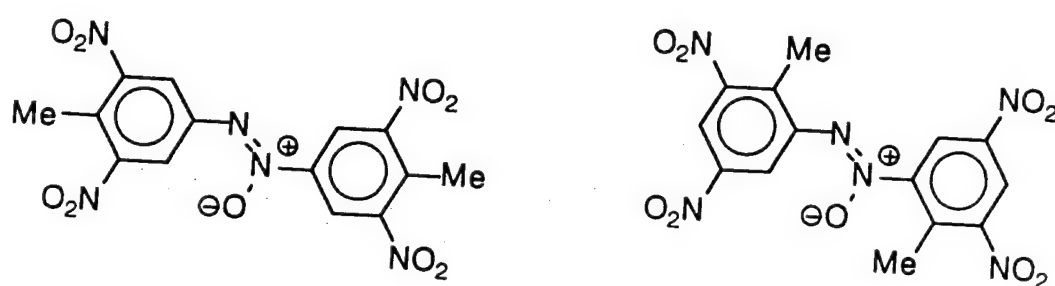


Figure 2-4B. Formation of Intermediate Azoxy Dimers.

## Degradation Factors

Researchers have shown that the degradation of explosive compounds is a direct function of environmental, biological, physical, and chemical factors affecting the compound whether it resides as a contaminant in the soil or is in solution in an industrial waste stream. Environmental factors include soil geology, ground water depth and flow, and climatic conditions such as precipitation and evaporation rates. Biological factors focus on the ability of both indigenous and exogenous microbial and vegetative populations to utilize the contaminant as an energy or nutrient source.

As researchers systematically control these factors in their research, the information collected will eventually chip away the barriers preventing restoration of contamination sites or effective treatment of industrial waste waters. Many researchers have used TNT labeled with radioactive carbon ( $^{14}\text{C}$ ) in order to track the contaminant's fate as various environmental, biological, physical, and chemical factors are adjusted during the study.

## Environmental Conditions

The environmental conditions placed on a contaminated site have a direct impact on the remediation processes that may or may not occur in the degradation of the contaminant. Under anaerobic conditions, the preferred degradation reaction is the reduction of the  $\text{NO}_2$  groups to  $\text{NH}_3$  groups. In

aerobic environments, the oxidation of the CH<sub>3</sub> group results in the formation of compounds such as trinitrobenzaldehyde, trinitrobenzoic acid, and TNB. It is speculated that azoxy compounds are formed when environmental factors uncontrollably change from anaerobic to aerobic conditions.

#### Biological Processes.

In the last twenty years, incremental advances have established specific fungal and bacterial populations capable of transforming explosives in laboratory environments. As researchers continue to understand the factors affecting these populations and the mechanisms involved, processes can be developed for full scale remedial implementation.

#### *Fungal Processes.*

The white rot fungus, *Phanerochaete chrysosporium*, has been receiving a lot of attention due to its ability to degrade xenobiotic, recalcitrant compounds. *P. chrysosporium* produces two unique extracellular enzymes; lignin peroxidase (LiP) and manganese peroxidase (MnP). These enzymes exhibit characteristics that enable it to degrade lignin and other recalcitrant compounds (Spiker et al. 1992). *P. chrysosporium* first received attention due to its ability to degrade wood and wood-preserving compounds such as creosote.

Fernando et al. (1990) grew white rot fungus in a matrix comprised mostly of corn cobs. The fungi-cob matrix was established to protect the fungi and

provide a stable growth environment. The matrix was mixed with TNT contaminated soils in hopes of degrading the TNT. They were moderately successful, 20% was metabolized to  $^{14}\text{CO}_2$  and 50% was transformed to water-soluble daughter compounds. Fernando increased the TNT concentrations to field conditions of 10,000 ppm soil and 100 ppm liquid. The indications from this study imply that high concentrations of TNT were not inhibitory to the fungi.

Spiker et al. (1992) conducted another study and determined that *P. chrysosporium* were unable to tolerate TNT concentrations greater than 20 ppm. This study utilized soils from the Umatilla Depot in Oregon contaminated with concentrations of 12,000 ppm TNT, 3,000 ppm RDX, and 300 ppm HMX. Concerned that the combination of explosives and indigenous soils may be inhibitory to the fungus, pure TNT was also tested. It was determined that TNT was inhibitory at concentrations higher than 20 ppm. Spiker also varied the stage of the life cycle of *P. chrysosporium*. Both Fungal spores and established mycelial growth were introduced to the soils at various TNT concentrations. TNT transformation products were identified as "more water soluble" intermediates. These water soluble intermediates were likely hydroxylamino and azoxy daughter products. Spiker's results support the work done by Fernando et al. (1990). If the fungus can be protected and immobilized on a host matrix, it may be able to degrade higher concentrations of TNT.

Valli et al. (1992) degradation research of 2,4- Dinitrotoluene by *P. chrysosporium* proposes specific degradation reaction pathways. Initial

degradation followed the  $\text{NO}_2$  reduction pathway to form intermediates of 2,4-diaminotoluene, 4-amino-2-nitrotoluene, and 2-amino-4-nitrotoluene. The last compound was observed in the greatest concentrations and became the object of further study. Valli identified the second stage fungal metabolites as 4-nitrocatechol, 1,2-dimethoxy-4-nitrobenzene, and 2,4-diaminotoluene. Additional degradation metabolites were also formed and are illustrated in Figures 2-5 and 2-6.

In the reaction pathways illustrated in Figure 2-6, both  $\text{NO}_2$  groups are removed before the aromatic ring is fractured. After the reduction of one  $\text{NO}_2$  group, the peroxidase oxidizes the contaminant to form an orthoquinone. Once this quinone is produced, the compound can then undergo a series of methylation and reduction cycles. Ultimately, DNT is transformed to 1,2,4-trihydroxybenzene and then to  $\beta$ -ketoadipic acid which is readily metabolized to  $\text{CO}_2$ .

### *Bacterial Processes*

McCormick et al. conducted several aerobic and anaerobic studies that identified several strains of *psuedomonas*, cell free *E. coli* enzymes (1976), and *Mucrosporium sp.* (1978) that were capable of transforming the  $\text{NO}_2$  groups of TNT to  $\text{NH}_3$  group intermediates. Cleavage of the aromatic ring was postulated to involve the further conversion of the  $\text{NH}_3$  groups to phenols. The production of phenols was not observed nor was there evidence of ring cleavage. The



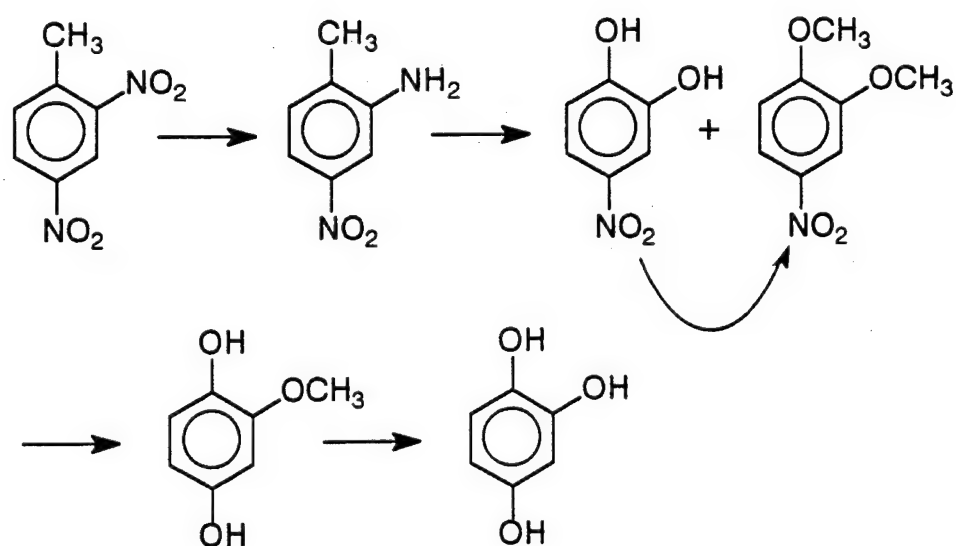


Figure 2-5. Degradation Reaction of 2,4-DNT by *P. chrysosporium*.  
(Valli et al. 1991)



consortia were capable of reducing two of the three  $\text{NO}_2$  groups to  $\text{NH}_3$  groups as described previously by the  $\text{NO}_2$  reduction pathway.

Bradley et al. (1994) investigated whether or not indigenous biological populations were responsible for degrading TNT from known surface contamination and causing TNT metabolites and daughter products to leach into the underlying aquifer and contaminate the ground water. Bradley used an inactive ammunition plant near Weldon Springs, Missouri to identify and confirm microbial activity and degradation products present in four different soil zones.

Bradley et al. (1994) concluded that the disappearance of the radio-labeled carbon ( $^{14}\text{C}$ ) test substrate was attributable to biological activity. Therefore, the ground water contamination was also the result of in situ biological activity. This study established that biodegradation is still possible in environments that inhibit fungal degradation processes.  $\text{NO}_2$  group reduction was the preferred reaction observed during Bradley's study.

Bausum et al. (1992) conducted laboratory studies on river bottom sediments to identify microbial populations that may degrade DNT (both 2,4- and 2,6- isomers). Microorganisms obtained from waters downstream of the Radford, Virginia ammunition plant were capable of directly metabolizing DNT. Cultures of the mixed bacterial populations were enriched and were able to utilize DNT as the sole carbon source. 2,4-DNT degrading microbial strains were isolated but not identified in the report. The 2,4- isomer consistently disappeared or was

metabolized at a higher rate than the 2,6- isomer. In laboratory conditions this was more pronounced than in natural waters. Radio-labeling revealed that 60% was mineralized to  $\text{CO}_2$ . Bausum et al. (1992) suggests that since increased microbial populations were observed, a significant amount of the remaining  $^{14}\text{C}$  must have been utilized in the production of biomass. Microbial populations also responded as a function of the DNT concentration available. At concentrations above 0.1 mg/l, populations increased. At concentrations below 0.1 mg/l, there was no significant growth of the microbial population. Bacterial growth in the enriched cultures was approximated using first order kinetics. Reductions of 2,4-DNT and 2,6-DNT exhibited mean second order rates of  $3.9 \times 10^{-10} \text{ ml} \cdot \text{cell}^{-1} \cdot \text{min}^{-1}$  and  $9.9 \times 10^{-10} \text{ ml} \cdot \text{cell}^{-1} \cdot \text{min}^{-1}$  in the laboratory, respectively. Bausum et al. suggested the slower degradation rates for the 2,6-DNT isomer were attributed to the lag time required for the microbial population to initiate growth.

Boopathy et al. (1994a) identified a consortium of *Pseudomonas* able to utilize trinitrobenzene as its sole nitrogen source. The most active bacteria in the consortium were identified as *P. fluorescens* and *P. Mendocina*. Both are gram-negative rod species. Individually, the pseudomona did not significantly metabolize the trinitrobenzene. When the entire consortia of soil bacteria were used, enzymes were produced that metabolized the TNB. Boopathy speculates the degradation of TNB to dinitroaniline, which would be consistent with other observed pathways (Won et al. 1974; McCormick et al. 1976; Kaplan and Kaplan

1982). Boopathy et al. (1994a) further suggests that the dinitroaniline is deaminated to form dinitrobenzene. Dinitrobenzene can be reduced again to form nitrobenzene. Nitrobenzene was observed as an end product accumulating in the culture medium during the study. An important aspect of this *Psuedomonas* consortium is that it was using the contaminant, trinitrobenzene, as a nitrogen source, leaving the aromatic ring intact, and releasing ammonia into the culture. This contrasts previous research because the release of nitrite had not been observed.

In a different study, Boopathy et al. (1994b) observed that a newly discovered methanogenic bacteria, *Methanococcus* sp. (strain B) transformed several nitroaromatic compounds. Boopathy and Kulpa (1993) isolated this specific bacterium from lake sediments. The bacteria was able to degrade the compounds: TNB, DNB, NB, 2,4-DNT, 2,6-DNT and 2,4-dinitrophenol. The bacteria reduced the contaminants co-metabolically when a primary electron donor and nitrogen source were supplied. Sulfide levels of 0.05 mM provided sufficient nutrients for all the methanogens studied. NO<sub>2</sub> reduction to NH<sub>3</sub> group end products was observed. In this report, Boopathy (1994b) cited a previous study (Boopathy and Kulpa 1993) in which *Desulfovibrio* sp. (B strain) reduced TNT to triaminotoluene (TAT). Triaminotoluene is very unstable and is quickly deaminated to toluene. This is important because remediation mechanisms for benzene and toluene are well known and not further discussed.

Funk et al. (1993) utilized an anaerobic procedure that has remediated soils contaminated with the nitroaromatic herbicide dinoseb (2-sec-butyl-4,6-dinitrophenol). Soil cultures were prepared from a soil inoculum obtained from a dinoseb-contaminated site in Ellensburg, Washington. The cultures contained aerobic heterotrophs capable of growing with respiratory inhibitors (TNT and dinoseb) and anaerobic organisms capable of degrading the dinoseb. Funk used TNT contaminated soils from the Umatilla Army Depot, Oregon. Indigenous bacteria were fed potato starch in order to induce anaerobic conditions in the soil cultures. The cultures degraded the explosive contaminants by transforming one of the  $\text{NO}_2$  groups to an  $\text{NH}_3$  group. Optimum anaerobic conditions were determined by varying the temperature and pH. Temperature ranges of  $20^\circ\text{C}$  to  $37^\circ\text{C}$  and pH ranges of 6.5 to 7 were cited as optimal. Elevated pH (anaerobic) conditions resulted in the formation of undesirable azoxy-dimers. Initial supplements of ammonium chloride were beneficial, as Funk noted that explosive contaminated soils are often nitrogen deficient or limited. As degradation occurs, the nitrogen demand lessens as ammonium is released from the hydroxylaromatic intermediates and is available to the cells.

Biological systems are a primary focus of the research community for remediating hazardous waste sites. Because biological systems are living organisms, their substance, growth, and decay, depends on a complex interaction between the climatic and ecological conditions to which they are

exposed. For instance, northern climates may require longer remediation times as most organisms go into a dormant state during low temperature conditions.

Also, because of the extensive research already conducted, many of the studies are being validated or refuted by other researchers as they try to implement or expand on previous works. Therefore, the timeliness of the research is very important as incremental advances are continuously being made. For instance, Funk et al. (1993) disputes Fernando et al. (1990) research that *P. chrysosporium* is capable of concurrently degrading both TNT at 12,000 ppm and RDX at 3,000 ppm at these concentrations. Funk's research, which confirms Spiker et al. (1992), indicates that concentrations above 0.02% wt/vol (200 ppm) significantly inhibit the degradation of TNT.

As researchers strive to definitively determine the reaction mechanisms and the supporting factors that will completely mineralize explosive compounds, their interest and enthusiasm is rekindled from the detection of small amounts of  $^{14}\text{CO}_2$ . This is significant in that there must be a mechanism occurring that is mineralizing the contaminant to this elemental compound. Although the presence of the radio labeled carbon dioxide ( $^{14}\text{CO}_2$ ) is promising, none of the literature reviewed identifies specific mechanisms that could be expanded upon and incorporated into a pilot or full-scale remediation system.

Finally, the ecological environment in which the biological populations inhabit requires that sufficient supporting factors do not become rate limiting.

While hoping that the contaminant will be utilized as the primary energy (carbon) source, other factors such as the amount of available electron acceptors and donors (oxygen and hydrogen), nutrients (such as phosphorus, nitrogen, & sulfur) must also be tracked and accounted for. Soils and sediments that contain less than 5 to 10% aerated pore spaces tend to exhibit microbial activity characteristic of anaerobic environments. This is primarily due to the low oxygen diffusion coefficient of the ground water (Bradley 1994).

In situ biological systems often demonstrate higher degradation efficiencies when indigenous populations are properly motivated to metabolize the contaminant in contrast to the introduction of an externally adapted bacterial consortium that may have difficulty just being adequately delivered to the contamination zone. The discovery of indigenous populations in freshwater systems downstream from an AAP near Radford, Virginia and soils from a fertilizer facility in Washington capable of at least partial degradation, indicate that organism adaptation is possible (Bausum et al. 1992 and Funk et al. 1993).

### *Vegetative Processes*

Vegetative processes are gaining strong favor due to a variety of remediation benefits. These benefits include increased depth of contaminant removal primarily due to root water uptake. Vegetation also increases the organic content of the soil. The root system and the increased organic content of the soil provide additional adsorption sites to which the contaminants can attach.



Finally, establishing vegetative cover minimizes contaminant dispersion and migration due to soil erosion by wind and water.

Banwart et al. (1991) determined the recovery effects of various plant species when treating TNT soils with the addition of organic residue amendments. When amendments were added to the contaminated soils, plants coped better against the contaminant-induced stresses. Rye grass demonstrated the most tolerance to the TNT compounds as it was almost indifferent to the percentage of amendments. All three plant groups, sorghum / Sudan grass mixture, alfalfa, and perennial rye grass, responded well to any combination of amended soils greater than 10%. Once the TNT was adsorbed, Banwart's analytical methods could not identify the fate of the compounds; either by removing or detecting them in the soil matrix or the plants' tissues.

Mueller et al. (1992) studied whether plant cells adsorbed, internalized, transformed, or metabolized the TNT contaminants. Initial results indicated that the cells did in fact internalize and convert the TNT into intermediate products described previously. Secondly, Jimson weed, *Datura innoxia* and *Datura quercifolia*, and a wild tomato plant species, *Lycopersion peruvianum*, were transplanted into known concentrations (500, 750, and 1,000 ppm) of TNT contaminated soils. After two weeks, the plants were removed and the concentrations of carbon labeled ( $^{14}\text{C}$ ) TNT intermediates were measured in the roots, shoots, and leaves. Root concentrations of degradation compounds were

as high as ten times (10x) that of the contaminated soil, while the amount of the raw TNT in the root was less than 10% of the total. Concentrations in the above ground plant sections were detected but not further enumerated. The Jimson weed, *D. innoxia*, tolerated concentrations of 1,000 ppm without exhibiting contaminant-induced stresses. Mueller believed that if the duration of the study were continued, more contaminant would have been translocated into the upper parts of the plant.

Skogerboe et al. (1991) conducted a study of surface runoff, and plant growth and bioaccumulation tests on an explosive ordinance site at a U.S. Navy submarine base in Washington. The establishment of vegetative covers on bare, TNT contaminated soils reduced suspended solids from 1,000 mg/l to 10 to 20 mg/l. Soil TNT concentrations tested were 3.3 mg/kg, 30 mg/kg, and 3,030 mg/kg TNT. Skogerboe established tall fescue on all the soils except the samples with the highest concentration.

The addition of soil amendments (horse manure) increases the plant's tolerance to the TNT. Good plant growth was observed at concentrations up to 900 mg/kg. Plant uptake determinations were not conducted due to poor recovery methods from plant tissues. Concentrations greater than 100 mg/kg severely inhibited the growth of tall fescue and may require soil amendments. Localized hot spots could be tilled to reduce the average concentration in order to establish grass cover. Finally, vegetative covers should utilize low preference

grazing plant species. This may discourage wildlife from grazing within the remediation zone. If this is not feasible, the use of high preference grazing vegetation should be planted elsewhere to attract them away from the area (Skogerboe et al. 1991).

Pennington et al. (1989) conducted a study that was unable to attribute any significant remedial degradation of explosives due to plant uptake. Pennington studied the contaminants TNT, 4ADNT, and 2ADNT from two soils, Sharkey clay and Tunica silt with the test plant yellow nutsedge. Contaminant concentrations were applied at 80  $\mu\text{g/g}$  of soil. Varying the pH at any of the treatment levels did not significantly increase plant uptake into the plant's leafy portions.

Pennington's study may only be able to suggest that clay and silty materials may not release the explosive from the soil matrix into the plant's structure. Harvesting of root material was not reported so as to determine the effect of adsorption from the soil matrix to the root structure nor were the roots tested for concentrations of explosives. This can be attributed to a couple of factors. One, the increased number of adsorption sites provided by the clean amendments and, two, the dilution factor of adding non-contaminated materials to the soil (Banwart et al. 1991).

Vegetative remediation processes offer a variety of benefits that make it attractive to explosive contaminated soils. The majority of explosive

contamination is surface contamination. Surface concentrations are typically an order of magnitude higher than deeper soil and ground water contamination levels. Once the vegetative population is established, the roots not only provide adsorption sites but also provide a contaminant sink which draws the explosive from the soil-water pore spaces. Previous research by Mueller did not identify the degradation compounds present in each of the plant sections. Additionally, research has not determined whether breakdown occurs as a result of photosynthetic processes. These questions illustrate the need for additional research that addresses these issues in a manner that permits engineers and remediation specialists to use the information productively.

#### *Ex Situ Biological Processes*

Composting. Composting is the only bioremediation process that has been tested in field-scale conditions. Currently, the U.S. Army is composting explosive contaminated soils at many of its ammunition plants. Composting is effective at reducing original TNT concentrations to oxidative and reductive intermediates, but has yet to demonstrate permanent binding of the intermediates within the soil-compost matrix. If this cannot be demonstrated, disposal as hazardous waste may be the ultimate result. This would be less economical than initial hazardous waste disposal due to the increased volume from the added compost ingredients (Williams et al. 1989, Griest et al. 1991, Majors et al. 1994, and

Kaplan and Kaplan et al. 1982).

Humification. Humification is a process that transforms compounds such as aromatics to naturally occurring humic and fulvic acids in the soil. Majors et al. (1994) postulates that this process may be likely if the soil environments are alternately rotated between anaerobic and aerobic conditions several times. This alternating oxidative environment may be able to provide the formation of imine bonds and secondary amine bonds.

A differing reaction process, that may achieve similar results is the reaction of the aromatic amine and quinones resulting in the formation of secondary amine bonds (Parris, 1980 as reported by Majors et al., 1994).

Soil Slurry Reactor. Manning et al. (1991) utilized a soil slurry reactor to reduce TNT concentration levels by about 90%. Aerobic and anoxic reactor configurations were alternated in order to reduce contaminant concentrations cometabolically. No further discussion or explanation of the mechanics or kinetics of the system were presented.

#### Physical / Chemical Processes

There are many physical / chemical processes that may be capable of treating waste streams and degrading contamination from explosives production, maintenance, and disposal operations. The majority are traditional treatment processes utilized for municipal and hazardous waste treatment. These include,

carbon adsorption, destruction by light (photolysis), composting, wet air oxidation, and incineration.

Photolysis. The most prominent natural physical / chemical process that degrades TNT is photolysis. Photolysis is the result of exposure to ultraviolet light or sunlight. Photolytic degradation is significant in the top few inches of contaminated soils and waste waters (Roberts, 1986). Formation of azoxy di-isomers, 2,2',6,6'-tetrinitro-4,4'-azoxytoluene or 2,2',4,4'-tetrinitro-6,6'-azoxytoluene, from the coupling of hydroxylamino and nitroso intermediates were observed (Spanggord et al. 1981, 1983). These di-isomers are dead end products that are much more resistant to further degradation than the nitro reduction or methylation intermediates.

Although hard to control, photolytic processes should be minimized to prevent excessive production of these recalcitrant di-isomers. These di-isomers may provide a contaminant reserve that slowly releases leachate affecting the ground water below.

Granular Activated Carbon. Freeman (1991) suggested that the only effective means of treating explosive manufacturing waste waters (Red Water) is the use of granular activated carbon (GAC). The high regeneration and disposal costs are GACs main problems. Regeneration facilities might have a problem of high reactivity while trying to regenerate the spent GAC. Therefore, disposal of spent

GAC as a hazardous waste is necessary. This has made explosive production very costly. In fact, the U.S. Army halted production of the explosives TNT, RDX, and HMX until an effective treatment method can be implemented to adequately dispose of red water waste streams (Freeman (1991), Hao et al. (1991), Majors et al. (1994), and Gorontzy et al. (1994)).

Wet Air Oxidation (WAO). Freeman (1991) and Hao et al. (1991) both suggest alternative processes, such as wet air oxidation, for effective treatment of TNT red waters. WAO is ideal, over incineration, for wastes with low solids (high liquids faction) content. WAO is a treatment process that utilizes high temperature, high pressures, and supplemental oxygen to break down the waste. Theoretically, WAO end products are CO<sub>2</sub>, water, nitrogen (or ammonia), and solids converted to their highest oxidative state.

Freeman further suggested incorporating powdered activated carbon (PAC) sludge treatment (PACT) with the wet air oxidation process. One of the major benefits of coupling the two technologies is that the PAC can be regenerated locally by the WAO process. Major disadvantages of the PACT / WAO system are the high costs associated with procuring and maintaining the equipment.

Incineration. Incineration is the ultimate destruction process in regards to hazardous waste. Incineration is not only expensive but negative public

connotations are always associated with it. Public concern aside, the total costs of incinerating explosive contaminated ammunition plant soils may be as high as \$1.5 billion. Normal costs are approximately \$300 to \$600 per ton for quantities less than 20,000 tons and \$200 to \$300 per ton for larger volumes (Williams et al. 1991).

All the physical and chemical processes ex situ techniques require physical removal of the contaminated soil or soil-water and processing it through a mechanical system. The main disadvantage is the very high cost associated with these systems.

On a final note, in support of incineration, it is the only process that is capable of breaking the contaminant down to elemental components. A slight drawback is that it also renders the waste (ash or soil) material virtually inert and sterile. Sterile soils are not desirable when restoring a site. Vegetation and biological systems are very difficult to reestablish in sterile soil matrices. Therefore, additional capital is required to augment the soil with natural amendments or other soil mixing techniques when restoration or replacement is desired.

#### **SUMMARY**

It is important to note that none of the cited research established a degradation step linking the removal of the nitro or amino groups from the



original compound. In other words, TNT has not been shown to degrade directly to DNT. Degradation experiments that recovered radio-labeled carbon dioxide could not establish a documented pathway to explain the cleavage of TNT's ring to elemental compounds.

The use of indigenous microbial populations has shown the most promise in remediating other hazardous waste sites. These same populations may require acclimation or a primary substrate source to serve as an electron donor or energy source in order for the microbes to at least co-metabolize the contaminant to elemental products or at least non-hazardous intermediates. Vegetative systems offer the additional benefit of minimizing the downward leaching of the contaminant into underlying aquifers and uncontaminated soils. They may also be capable of reversing the leaching effects due to the plant root's ability to attract, internalize, uptake, and possibly transform the contaminant.

## **CHAPTER 3.**

### **DEVELOPMENT OF THE MODEL**

Today, in situ remediation methods are the most desirable choice in remediating hazardous waste sites over traditional methods of ex situ processes of the last 25 years. Ex situ processes are well known for their overwhelming capital requirements and manpower intensity. Colossal efforts and high costs associated with excavation, transportation, and disposal operations were often the "norm." In situ processes, on the other hand, exploit natural processes and often enhance indigenous biological systems to detoxify the antagonistic hazardous compound. In situ processes, when viable, are often more efficient and effective at reclaiming the contaminated area to a useful purpose.

One common problem associated with in situ remediation is that it is very difficult to visibly confirm that degradation is occurring. Through the use of monitoring systems, real time sensors, and analytical models, in situ remediation can demonstrate remedial restoration without visible on-site excavation and disposal operations.

Remediation models are used for two very distinct reasons. The first is to demonstrate the expected results of all the various alternative remediative processes hypothesized during the Remedial Investigation / Feasibility Study (RI/FS) process. The RI/FS model should predict and provide an understanding

of the fate and transport of the target contaminants through the affected soils and water (surface and ground) systems and identify critical environmental and holistic community resources at risk. The second is to integrate the theoretical and scientific concepts with data obtained from the field. This integration results in real time monitoring of the in situ reactor and tracking the progress of the remediation project. In situ systems are difficult to monitor because the reactor vessel has many unknown variables that are often assumed because they are difficult to define. Maintaining sufficient balance of electron acceptors, nutrients, and moisture within the in situ reactor can be a challenge. Each in situ reactor has unique characteristics that require competent process knowledge of the physical, chemical, and biological mechanisms involved. Otherwise, ineffective treatment will occur that may prevent further in situ processes from being re-initiated.

#### ***DEVELOPMENT AND DESCRIPTION***

This thesis will utilize the model, BIOROOT, to monitor the fate and transport effects of TNT contamination at the Umatilla Depot in northern Oregon. BIOROOT has been used to model the transport of a conservative contaminant in two dimensions through a variably saturated soil (Tracy et. al. 1992, 1994). The model solves a series of second order partial differential equations using a Galerkin finite element solution technique that employs quadratic isoparametric elements and a Crank-Nicolson difference method for the time derivative

interval. BIOROOT assumes the target contaminants will be transported through a porous media following an advective-dispersive behavior. The model assumes that the adsorption capacity of the soil behaves linearly and is a function of the bulk density of the soil. The contaminants are also assumed to be influenced from biological effects including microbial populations and vegetative processes. However, if limited contaminant degradation information is available, the degradation can be simulated as a first order decay process.

Specific parameters relating to the soil, plant, and microbial species should be obtained from either laboratory experiments, field surveys, or estimated from known reference data through a variety of methods (Zappi et. al. 1991, Lyman et. al. 1982, Howard et. al. 1991.)

The governing mass balance equation for the fate of a contaminant in BIOROOT is shown below:

$$\frac{\partial}{\partial x} \left[ \theta \left( D_{xx} \frac{\partial C}{\partial x} + D_{xz} \frac{\partial C}{\partial z} \right) - V_x C \right] + \frac{\partial}{\partial z} \left[ \theta \left( D_{zx} \frac{\partial C}{\partial x} + D_{zz} \frac{\partial C}{\partial z} \right) - V_z C \right] - (qT_{scf} + k)C = \frac{\partial [C(\theta + R_d R_{cf} + \rho_b k_1)]}{\partial t} \quad (1)$$

Where:

$\theta$	soil-water content
$\rho_b$	bulk density of the soil
$C$	solute concentration
$D$	Dispersion coefficient
$k$	first order decay rate
$k_1$	adsorption coefficient
$K_r$	hydraulic conductivity of the root
$K_s$	hydraulic conductivity of the soil
$q$	soil-water extraction rate by the plant's root system

$R_d$	density of the root mass in the soil volume
$R_{cf}$	root concentration factor
$t$	time
$T_{scf}$	plant's transpiration stream concentration factor
$V$	Darcy soil-water flux
$x$	horizontal spatial dimension
$z$	vertical spatial dimension

The dispersive-advective effects ( $\theta D_{ii} \partial C / \partial i$  and  $V_i C$ , respectively) are represented by the partial differentials in the horizontal ( $x$ ) and vertical ( $z$ ) dimensions. The contaminant sink ( $-q T_{scf} C$ ) from the plant's uptake of the contaminant and the rate of contaminant decay ( $-kC$ ) complete the mass balance of the contaminant entering and leaving the control volume.

The right hand side of the equation expresses the change in the mass balance of the contaminant within the soil control volume with respect to the temporal dimension. The total contaminant mass flux is equivalent to the change in concentration within the soil-water ( $C\theta$ ), the amount sorped onto the root structure ( $CR_d R_{cf}$ ), and that sorped onto the soil particle ( $\rho_b k_1 C$ ). The model also assumes that linear isotherm adsorption models adequately simulate the contaminants adsorption ( $k_1$ ) to the soil particles.

#### **ADDITIONAL RELATIONSHIPS**

Plants have an ability to adsorb and transfer hazardous organic compounds into its transpiration stream. The contaminant concentration in the transpiration stream ( $C_{ts}$ ) is a direct function of the plant's transpiration

concentration factor ( $T_{scf}$ ) and the solute concentration ( $C$ ) as shown (Tracy et al. 1994).

$$C_{ts} = T_{scf} C \quad (2)$$

$T_{scf}$  is, in turn, a function of the contaminant's octanol-water partition coefficient,  $K_{ow}$  (Briggs et al. 1982).

$$T_{scf} = 0.784e^{\left(\frac{-(\log K_{ow} - 1.78)^2}{2.44}\right)} \quad (3)$$

The root system not only provides additional adsorption sites onto the root structure itself but is also responsible for removing the contaminants from the soil matrix and transporting the contaminants into the plant's upper stem and leaf structure. Therefore, the plant provides a sink ( $S$ ) for the contaminant. The contaminant sink is a function of the plants' intake of the contaminated soil-water flux ( $q$ ) and the root transpiration stream concentration ( $C_{ts}$ ) from equation 2.

Rewriting equation 2 yields:

$$S = -qT_{scf} C \quad (4)$$

The adsorbed concentration ( $C_r$ ) onto the root structure is the product of the root concentration factor ( $R_{cf}$ ) and the solute concentration:

$$C_r = R_{cf} C \quad (5)$$

Again the root concentration factor demonstrates a functional relationship with octanol-water partition coefficient (Briggs et al. 1982).

$$R_{cf} = 0.82 + 10^{(0.77 \log K_{ow} - 1.52)} \quad (6)$$

The model also assumes that the soil-water content is a function of the soil-water pressure head (Brutsaert, 1966).

$$\theta = \eta \frac{A}{A + (-\psi)^c} \quad (7)$$

Where:

$\eta$  soil porosity  
 $\psi$  soil water pressure head  
 $A, c$  soil characteristic parameters

The soil hydraulic conductivity is a function of the soil-water content ( $\theta$ ) and the term  $d$ , which is another soil characteristic (Brooks and Corey, 1966)

$$K_s = K_{sat} \left( \frac{\theta}{\eta} \right)^d \quad (8)$$

Where:

$K_s$  effective hydraulic conductivity of the soil  
 $K_{sat}$  saturated hydraulic conductivity of the soil.

Equations 9 and 10 apply the distribution of the soil-water pressure head using Darcy's law to determine the water flux in the vertical and horizontal components as:

$$V_x = -K_{s_x} \frac{\partial \psi_s}{\partial x} \quad (9)$$

$$V_z = -K_{s_z} \frac{\partial (\psi_s + z)}{\partial z} \quad (10)$$

Where:

$\psi_s$  soil water pressure head  
 $V_x$  Darcy soil-water flux in the x dimension

## CHAPTER 4.

### SITE CHARACTERIZATION

A hazardous waste site near Hermiston, Oregon was chosen as the site to demonstrate the BIOROOT model's ability to simulate the fate and transport of the contaminant through the soil and groundwater. Normal environmental conditions with various remediation technologies is compared to a "No Action" alternative of the remediation process. The site is a U.S. Army munitions facility known as the Umatilla Depot Activity (UMDA). UMDA is a US Army facility being closed under the Department of Defense's Base Realignment and Closure Program and has been the focus of numerous environmental remediation investigations and feasibility studies to determine the extent of the environmental cleanup required to return the facility and associated land to the public and private enterprise.

Characterization information and parameters particular to this site were obtained from technical reports prepared by Dames and Moore (1994) and Morrison Knudsen Environmental Services and CH2M Hill (MKES et al. 1992) for the US Army Corps of Engineers Toxic and Hazardous Materials Agency.

#### ***SITE BACKGROUND.***

The UMDA complex had an explosives washout facility that was operational for 15 years from 1950 to 1965. Washout operations are best



described as a hot wash water and steam cleaning system that removed the explosive compounds from the various munitions' components. On a weekly average 150,000 gallons of wash water were discharged to a lagoon system (See Figure 4-1). Ultimately, estimates of approximately 85 million gallons of explosive wash water had been impounded in the lagoons.

#### ***SITE LOCATION AND DESCRIPTION.***

UMDA is located in the upper northeastern region of the state, located three miles south of the Columbia River. The Columbia River provides a portion of the north-south border with the state of Washington. The city of Hermiston, Oregon is located east of the depot. The washout lagoons are located in the central portion of the UMDA complex. The lagoons are located in a general area of a depression that slopes northeasterly toward the Umatilla River. The original lagoon system consisted of two lagoons each being 80 feet long with the north lagoon being 39 feet wide and the south lagoon being 27 feet wide. Typical depths average 6 feet. The lagoons were constructed with gravel side and central berms and sandy bottoms. The berms are 15 feet wide at the top and have side slopes of 35°.

#### ***CLIMATE.***

The climate for this region has been identified as a cold, semi-arid desert. Annual precipitation averages 8 to 9 inches, while evaporation averages 32

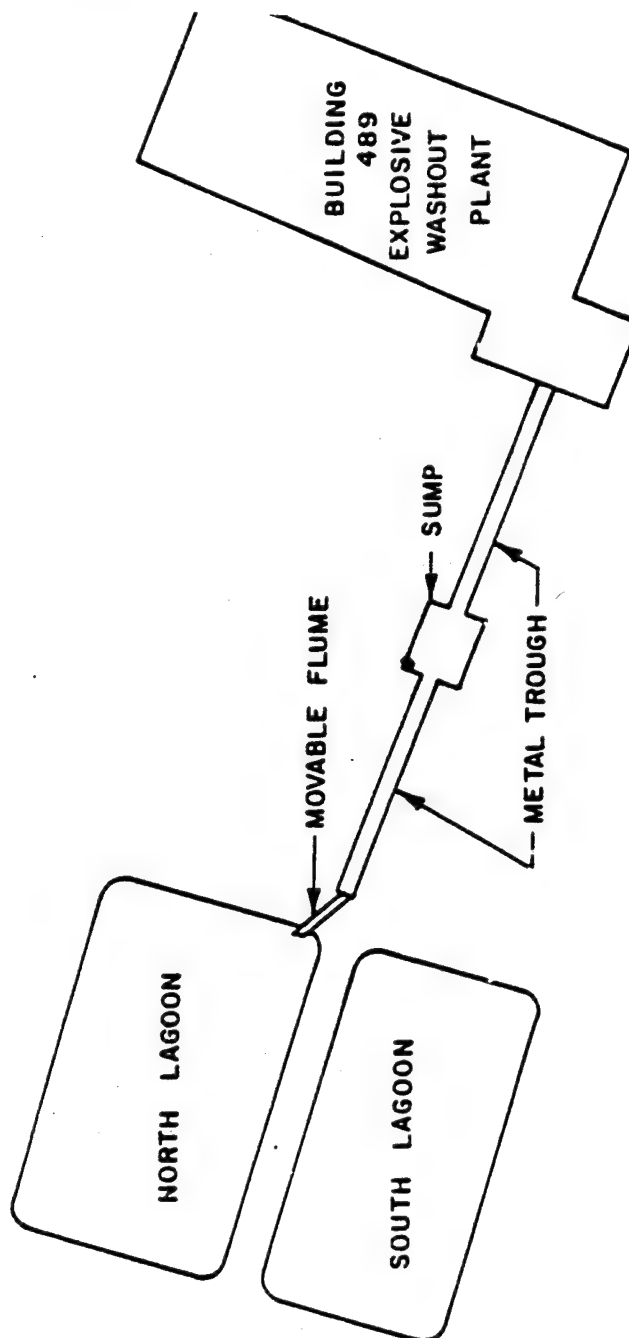


Figure 4-1. Explosives Washout Lagoon,  
Umatilla Depot Activity, Oregon  
(MKES et al. 1991)

inches. Vegetative species typically consist of arid grasses and shrubs. Temperatures range from -31°F to a maximum of 113°F. Average summer temperature is 75°F while the average winter temperature is 35°F (MKES et al. 1992).

#### **GEOLOGY.**

The underlying soils are glaciofluvial flood sediments, which are highly permeable. Surface drainage is poorly developed due to the ground surface's high permeability. The soils beneath UMDA are predominately from two major geologic formations. The upper soil formations are a glacial flood gravel and the underlying bedrock formation is known as the Columbia River Basalt formation. The glacial flood gravels range in thickness up to 200 feet and thin out at the slopes of the valley. Figure 4-2 illustrates the geologic profile of the greater Umatilla area (MKES et al. 1991). The Umatilla Depot is located on a thicker region of the flood gravel deposit. The flood gravel deposit forms an unconfined aquifer with a saturated thickness of at least 40 feet in the vicinity of the lagoons. Depth to the unconfined aquifer has been measured from 40 to 50 feet below the ground surface. The thickness of the basalt formation was not reported. However, the southeastern corner of UMDA contains the highest elevation of the formation at 490 feet. The basalt has a general slope toward the northwest.

Finally, the confined aquifers beneath UMDA are formations comprised of interbeds between unweathered basalt flows. The upper system is the Selah

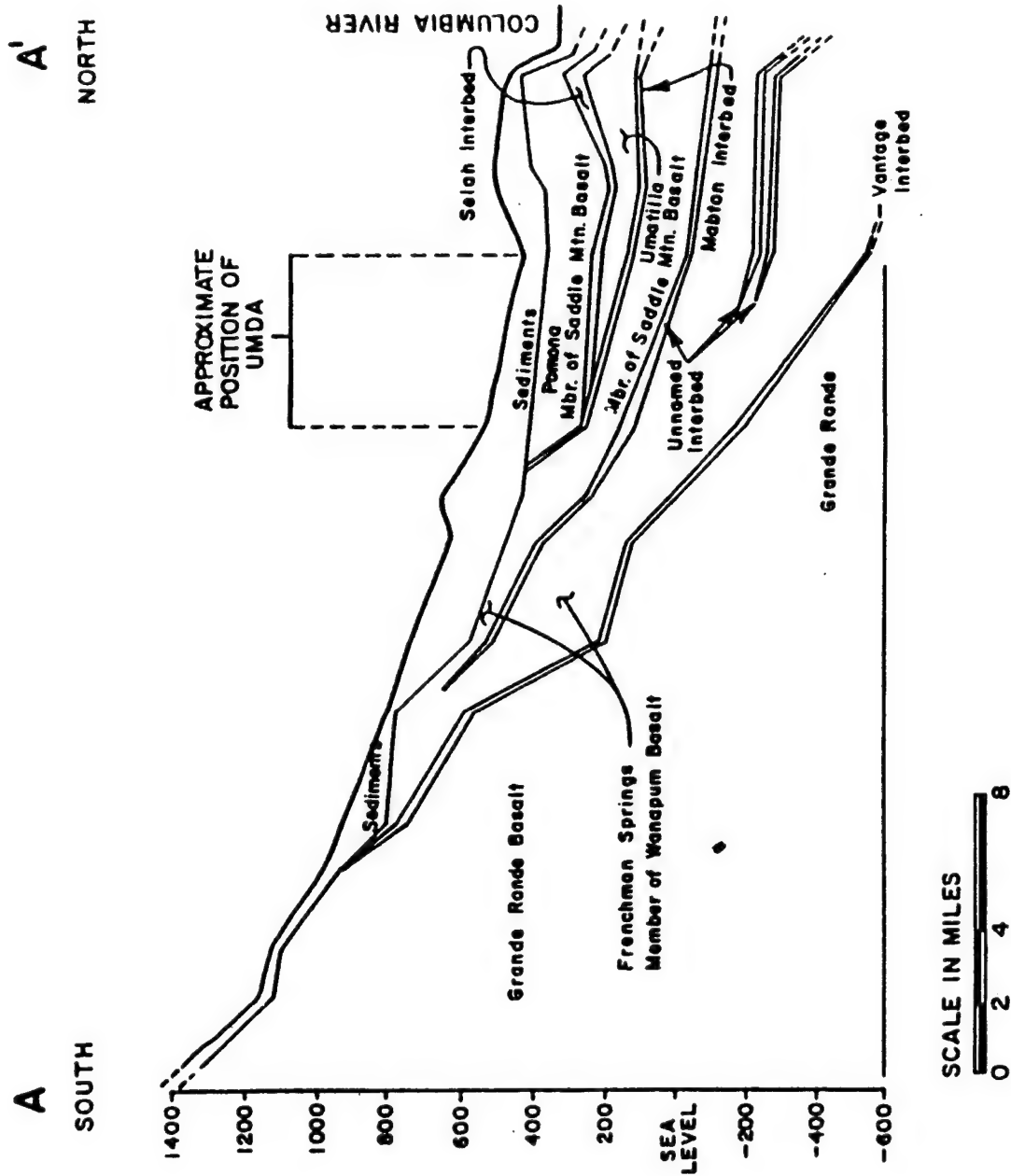


Figure 4-2. Subsurface Geology  
Morrow County, Oregon  
(MKES et al. 1991)

Interbed and the upper confining layer is identified as the Pomona Member of the Saddle Mountain Basalt formation which consists of weathered and unweathered basalt. It is generally believed that the confined aquifers are recharged from the higher sloped regions. None of the cited references (within MKES et al. 1992) suspected or identified that any of the confined aquifer systems were contaminated from the washout lagoons.

The direction and magnitude of flow from any of the ground water sources were not specified. Discharge to the Columbia River is likely and discharge from natural springs along the Umatilla River suggest natural ground water flows to be north by northeasterly toward one of the two river systems. Ground water pumping is suspected of controlling and reversing the ground water's flow as explosives contamination now appears to be migrating south by southeast. No specific reason was mentioned for this pumping whether it be for drinking water or for remediation purposes.

#### ***CONTAMINATION PRESENT.***

Previous supporting work (Weston, Ana-Lab Corporation, Century Environmental, Batelle, and Dames & Moore reported by MKES et al. 1992) identified the major contaminants as 2,4,6-TNT, 2,4-DNT, 1,3,5-TNB, HMX, RDX, nitrate and nitrite contamination. Explosive compounds were detected in the soil surrounding and beneath the lagoons. In addition to the explosives, nitrates and nitrites were detected only in the ground water. The greatest

concentrations of TNT were measured in the first 2 feet below the ground surface and ranged from 520 to 1,400  $\mu\text{g/g}$ . Localized "hot spots" were as high as 38,000  $\mu\text{g/g}$  but were generally less than 9,000  $\mu\text{g/g}$ . Detected levels of TNT decreased significantly from 1,400  $\mu\text{g/g}$  to as low as 1  $\mu\text{g/g}$  at depths of 10 to 12 feet. Depths greater than 12 feet exhibited concentrations not exceeding 50  $\mu\text{g/g}$  down to the water table (~50 feet). Figures 4-3 and 4-4 plot the depth of TNT concentration inside the lagoons from boreholes that cross-sectioned the lagoon system.

#### ***SOIL CHARACTERISTICS.***

General soil characteristics for the first ten foot depth in the explosive washout lagoon area are summarized in Table 4-1. The soil parameters reported are: alkalinity, pH, moisture content, and total organic carbon (MKES, 1992). The pH range, 7.6 - 8.4, was very tight, while the moisture content ranged from 3.5% to 17.5%.

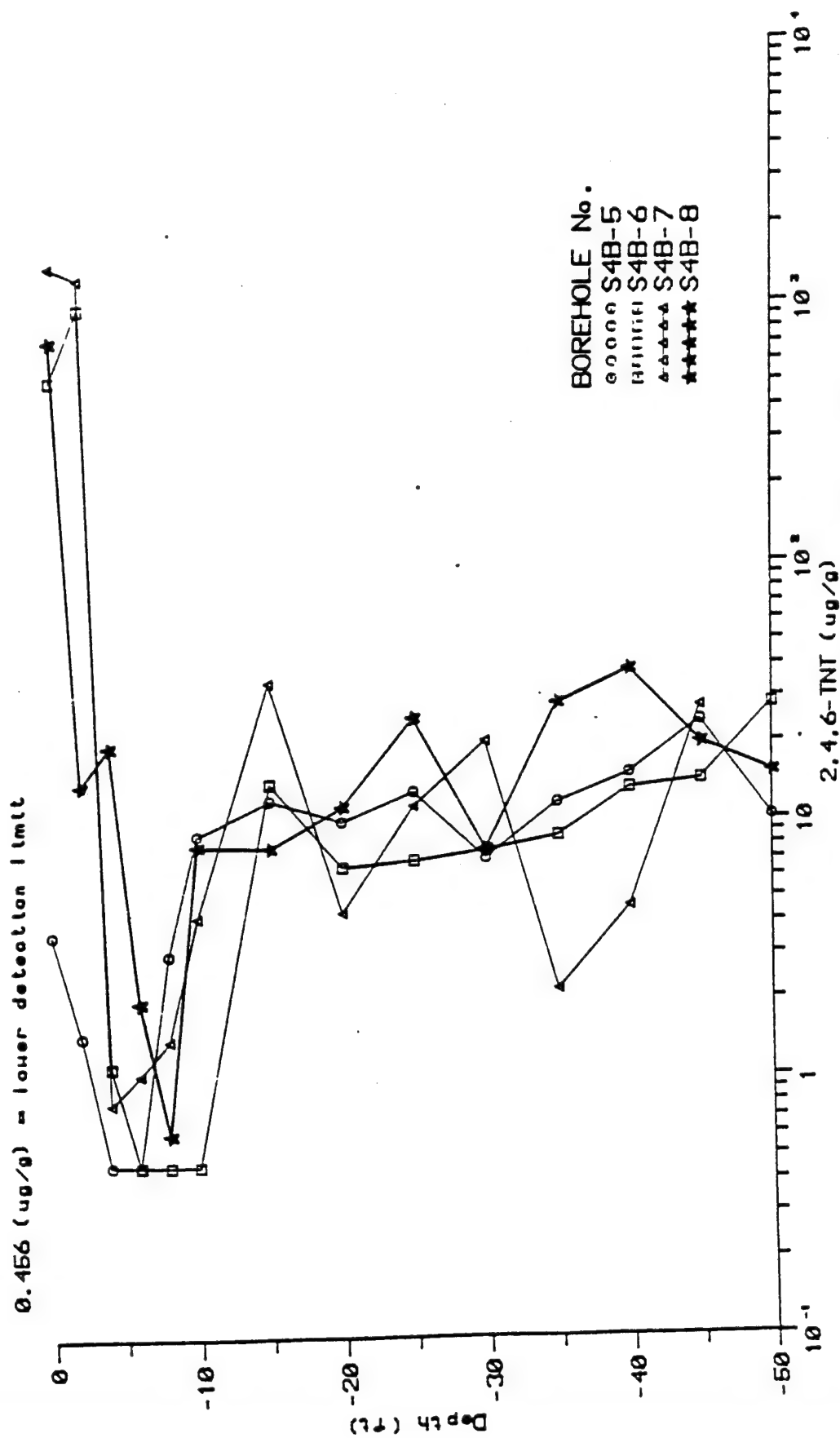


Figure 4-3. Depth vs Concentration of 2,4,6-TNT in Soil Explosive Washout Lagoons (log scale)  
(MKES et al. 1991)

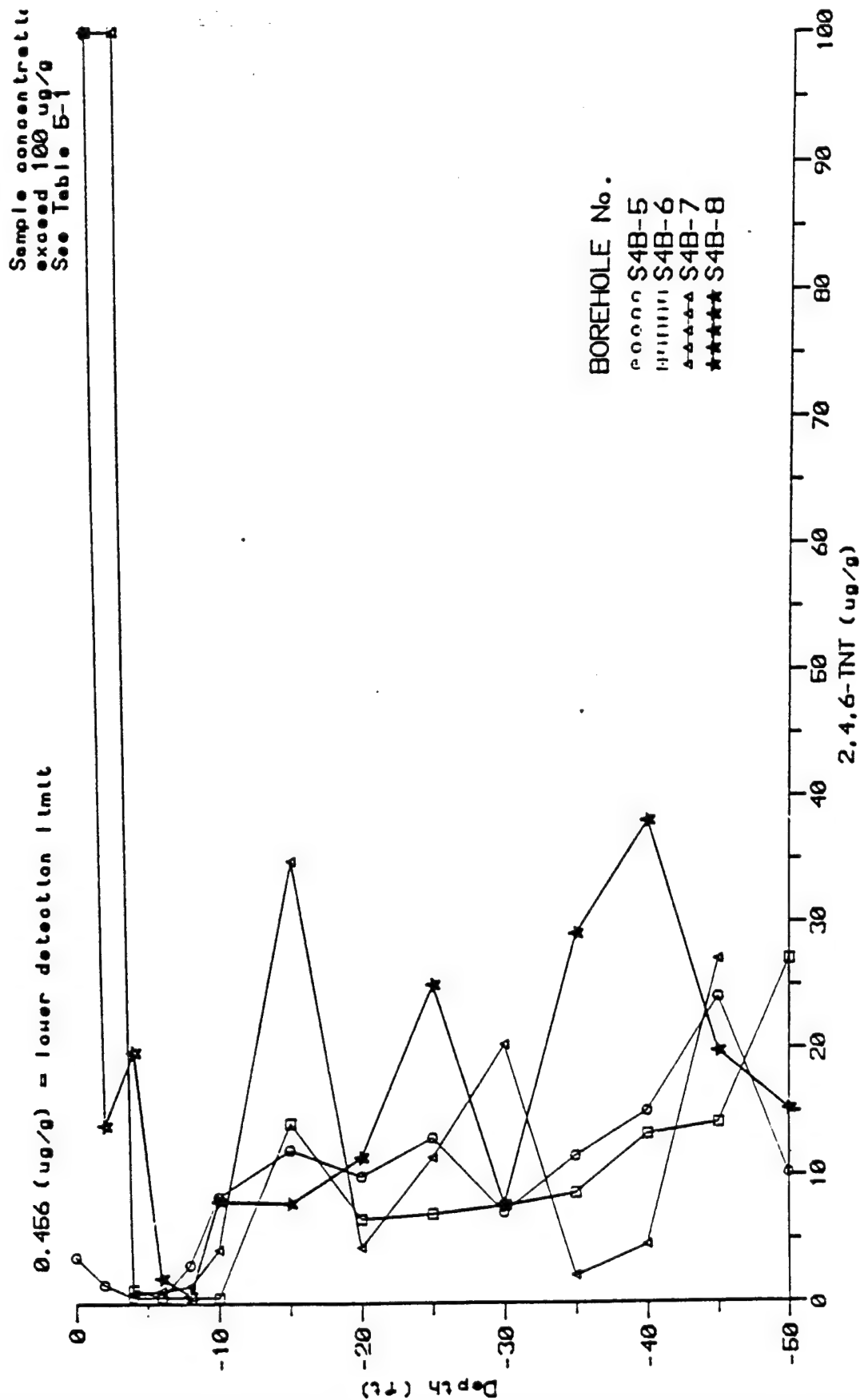


Figure 4-4. Depth vs Concentration of 2,4,6-TNT in Soil  
Explosive Washout Lagoons  
(MKES et al. 1991)



**TABLE 4-1. SHALLOW SOIL CHARACTERISTICS FOR  
UMATILLA EXPLOSIVE WASHOUT LAGOONS  
(DAMES & MOORE, 1991)**

<b>SITE ID</b>	<b>DEPTH (feet)</b>	<b>ALKALINITY<sup>A</sup> (µg/g)</b>	<b>PH</b>	<b>MOISTURE CONTENT (%)</b>	<b>TOC (g/kg)</b>
<b>S4B-5</b>	0	<25	7.64	4.7	0.892
	4	48	8.19	4.8	3.33
	10	52	8.11	7.1	0.808
<b>S4B-6</b>	0	102	8.27	5.2	7.34
	4	46	8.19	5.4	3.6
	10	50	8.11	16.7	1.42
<b>S4B-7</b>	0	194	8.35	5.3	4.88
	4	50	7.87	17.5	3.12
	10	66	8.08	6.6	2.19
<b>S4B-8</b>	0	54	8.2	3.5	1.93
	4	50	8.4	5.4	1.18
	10	194	8.3	4.7	0.841

<sup>A</sup> Alkalinity = Total Carbonate alkalinity (µg/g).

## CHAPTER 5.

### MODEL PARAMETERS

The BIOROOT model utilizes a finite element method for estimating the fate and transport of a contaminant through the soil profile. This requires developing a grid system that breaks down the soil profile into specific regions that mass balance relationships can be applied. The model also requires that specific soil parameters be known or estimated.

#### ***SPATIAL DEVELOPMENT OF FINITE ELEMENT MODEL.***

The two lagoons of the explosives washout facility represent an area of roughly 6400 feet square within the berms. Soil samples indicate that there are areas of significant contamination outside the bermed area.

The RI/FS reports indicate the soil's contaminant concentration profile has the highest measured values in the first two feet. Contaminant concentrations decrease significantly within in the top ten feet and return to a nominal concentration within the seasonal variations of the water table. Just above the water table it is believed that the water table behaves like a contaminant source to the immediately overlying soil formations (MKES et al. 1991).

The finite element method utilized by BIOROOT incorporates a spatial grid that has three horizontal nodes spaced within one meter. The horizontal dimensioning will permit the evaluation of the site based on a elemental unit

area equivalent to 1 square meter. The vertical orientation subdivides the first meter in quarters, the next two meters are divided into  $\frac{1}{2}$  meter increments, and the remaining depth is divided at an even 2 meter distribution to a total depth of 25 meters (approximately 80 feet). The water table was reported to be approximately 15 meters (50 feet) below the ground surface. Figure 5-1 illustrates the fundamental vertical spacing of the elements implemented for this study.

This elemental and nodal representation of the UMDA washout facility demonstrates the ability of the BIOROOT model in simulating the contaminant transport through the zone of interest. The hydraulic conductivity reported for the UMDA soils vary considerably between the various consultants. MKES et al. (1991) reported values approaching 277.44 feet per day (84.6 m/day) and the District Corps of Engineers (1992) reported values up to 3247 feet per day. These values are indicative of clean sands and gravels (Freeze and Cherry, 1979).

#### ***BOUNDARY CONDITIONS.***

The boundary conditions affecting the finite element model are the initial known heads of the unconfined aquifer. The magnitude and direction of the ground water flow were not cited sufficiently in any of the literature to incorporate realistic assumptions into the model. Therefore, the precipitation and evaporation data represent the only sources of known water fluxes in the model.

Nodes	Elements		Nodes	Depth (m)	Sandy Soil
1			3	0.00	
4	1	20	6	0.25	
7	2	21	9	0.50	
10	3	22	12	0.75	
13	4	23	15	1.00	
16	5	24	18	1.50	
19	6	25	21	2.00	
22	7	26	24	2.50	
25	8	27	27	3.00	
	9	28			
28			30	5.00	
	10	29			
31			33	7.00	
	11	30			
34			36	9.00	
	12	31			
37			39	11.00	
	13	32			
40			42	13.00	
	14	33			
43			45	15.00	
	15	34			
46			48	17.00	
	16	35			
49			51	19.00	
	17	36			
52			54	21.00	
	18	37			
55			57	23.00	
	19	38			
58			60	25.00	

**Figure 5-1. Finite Element Method Development  
Original Conditions**

**INITIAL CONDITIONS.**

As stated earlier, the surface contamination of TNT was measured at 500 to 1,400  $\mu\text{g/g}$  soil. Localized hot spots were identified at concentrations exceeding 35,000  $\mu\text{g/g}$ . For the purposes of this study, initial concentrations were averaged over the entire model area.

TNT concentrations in the deeper soils were measured at less than 50  $\mu\text{g/g}$  soil. Soil-water concentrations of TNT were approximated using the following relationship:

$$\log C_s = \log K + 1/n \log C_e \quad (12)$$

Where the  $K \approx 1.08$ , and  $1/n \approx 0.83$ . A plot of this equation on log-log paper results in a straight line where  $K$  is the y intercept and  $1/n$  is the slope of the line.  $C_s$  is the concentration adsorbed onto the soil particle and  $C_e$  is the amount of contaminant in solution (Environmental Sciences et al. 1991).

TNT is very recalcitrant and has a natural decay rate that Howard et al. (1991) reports as being from 4 weeks to 180 days. This is based on Spanggord's studies of freshwater organisms and does not directly apply to the application at hand. Therefore, a more conservative half-life decay rate of 360 days was assumed for the initial degradation simulation.

**TEMPORAL MODEL DEVELOPMENT.**

After establishing the spatial elements of the grid system and the initial and boundary conditions of the modeled system, development of the temporal

parameters are necessary. Influencing factor(s) that have the most effect on determining the period of time to simulate in the model are most often related to reported climatological data.

Climatological data required for the model included monthly precipitation, evaporation, and temperatures. This type of climatological data is often available from the state climatologist. Precipitation data received for this study dated from 1947 to present, evaporation data reported was "hit and miss" in completeness, and temperatures were complete except for minor instrumental errors resulting in non-recordings.

Arid regions typically have short duration storm events. Even though the average annual precipitation is less than 10 inches, the combination of storm duration, intensity, and soil permeability contribute to storm events producing localized runoff conditions. The amount of runoff is not accounted for by the climatological recording devices. Therefore, an estimate of the amount of infiltration being adsorbed into the soil was used. An incremental approach was implemented to determine the amount of precipitation that infiltrated the washout lagoon soils. For each half inch increment of rain received a 10% loss was incurred after the first half inch of rain. The initial quantity (0.5") of water infiltrated at 100%, the second increment infiltrated only 90%, and so on. In general, an overall reduction of 9 to 12% could be applied to all the monthly precipitation measurements. Climatic Data for the last eleven years was utilized and the adjusted and raw climatic data are attached in Appendix C.

**CONTAMINANT PARAMETERS.**

The model will use TNT as the primary contaminant. Knowing the intrinsic properties and behavioral characteristics of TNT with the surrounding environmental conditions are necessary to adequately model the degradation effects in the contamination zone.

Specifically, contaminant parameters such as solubility and partitioning coefficients describe how the chemical distributes itself between two mediums. Three partitioning coefficients are important to waste managers and remediation professionals. These are the octanol-water partition coefficient ( $K_{ow}$ ), soil-water partitioning coefficient ( $K_p$ ), and the vapor-liquid partition coefficient. BIOROOT utilizes the octanol-water partition coefficient as its main parameter affecting the contaminant interactions with the surrounding environment (LaGrega et al. 1994). The octanol-water partition coefficient is a dimensionless constant defined by:

$$K_{ow} = \frac{C_o}{C_w} \quad (13)$$

Where the ratio of the concentration of the chemical in octanol,  $C_o$  is compared to the chemical's concentration in water,  $C_w$ . This octanol-water relationship has been further expanded upon to make estimates concerning other parametric factors such as the root concentration factor and the plant's transpiration stream concentration factor. Once these two parameters are

known, the concentration of the contaminant in the structure of the plant can be determined from Equations 3-2 and 3-5 as described earlier.

Another important factor impacting the degradation of explosive compounds is their relatively long half life in natural environments. Simply stated, half lives are the amount of time required for the compound to degrade to half of the compound's original concentration. Most of the half-lives for explosive compounds are not known or are estimates derived from other environmental conditions. For instance, the half-lives for TNT are based on freshwater conditions. Therefore, applying these parameters to different environmental conditions is, at the least, slightly suspect.

#### ***ADSORPTION ISOTHERM COEFFICIENTS.***

The geotechnical profile indicates that the soil is a highly permeable sand with very low organic content. The organic content and adsorption potential is documented through Environmental Science's (1991) adsorption studies of the UMDA soil in which the Fruendlich adsorption isotherm values indicate coefficients of ~1.08 and organic contents of ~0.07% were found. Adsorption coefficients and organic contents in this range do not present a very adsorptive environment for the contaminant to become attached. Therefore, highly permeable sand with very low organic content contributes to a highly mobile advective transport of the contaminant. Contaminant transport is only hindered



upon reaching the saturated zone or when non-flowing conditions exist in the soil-water pore volume.

#### ***VEGETATION.***

The presence and density of arid vegetation is not well documented in the RI/FS reports. The only vegetation reference is to arid grasses and shrubs that exist in the general area. For the purposes of this study, it will be assumed that arid vegetation contributes to the organic factor (adsorption sites) of the upper soil, thus conservatively retaining more contaminant than ordinarily incorporated into the model.

#### ***Root Parameters.***

There are three main components of the plant that are involved with the uptake and transformation of contaminants from the soil. The most important aspect of the plant is the root system. Root systems vary a great deal between plant species. Plants with a higher density of root mass per unit volume of soil provide a greater amount of adsorption sites for the contaminant within the soil matrix.

#### ***SIMULATION SCENARIOS.***

In order to demonstrate the various remedial effects of contaminant decay, amendment addition, and vegetative uptake on the contaminant, four scenarios were simulated using the BIOROOT model. Temporal durations were based on monthly climatic data (Taylor, 1995). Monthly inputs for a total duration of 11

years were used in the model, providing adequate temporal and climatic variability to demonstrate the likely transport of the contaminant through the defined spatial system.

#### Scenario 1: No Degradation.

In the first scenario initial surface contamination is equal to 1,400  $\mu\text{g/g}$  in the first 0.5 meters (2 feet) of the soil. No initial contamination is present beneath 0.5 m. The degradation rate of the contaminant is zero so that no effective degradation occurs. The only factors affecting the fate and transport of the TNT are the advective-dispersive transport resulting from the infiltration of rain water. This scenario demonstrates whether the contamination in the surface soils is a likely contaminant source to the underlying soil and ground water and is the baseline scenario to be compared to the other simulations.

#### Scenario 2: Degradation with a Half Life of 1 Year.

The second scenario analyzes the effect of changing the degradation of the contaminant from no degradation to a half-life of 1 year. The effects of this change illustrates the remedial impacts associated with properly applied degradation rates of the model.

#### Scenario 3: Addition of Soil Amendments.

The effects of amending the soil with 10% organic material as demonstrated by Banwart et al. (1991) shall provide increased adsorption sites

and the minimum soil matrix that will support vegetative growth. Organic soil amendments are added to the top 3 feet of soil which has a slight dilution effect on the soil-contaminant concentration. However, the Initial concentration will not be reduced according to the linear dilution relationships in order to directly compare the results between the various scenarios. The 10% organic soil amendments will increase the adsorption characteristics of the soil by providing additional adsorption sites for the contaminants to attach. This amendment increase has been artificially represented as a soil having characteristics of a "sandy loam" soil for the model. Figure 5-2 illustrates the changes in the spatial development from the addition of soil amendments (sandy loam) to the area of interest which will also influence the test scenarios 3 and 4. Maximum amendment augmentation does not exceed 10% as no additional benefit to the remediation effectiveness in establishing plant growth was determined (Banwart et al. 1991) and costs associated with introducing external ingredients to the soil are minimized.

#### Scenario 4: Establishing Remedial Vegetation.

As stated above, the amendments to the soil provide a soil matrix that is more conducive to establishing vegetative populations, such as alfalfa (Banwart et al. 1991). The addition of vegetative remediation to scenario 3 demonstrates the overall effects of incorporating vegetative degradation in the upper soil contamination zone and evaluating whether vegetation is capable of minimizing

Nodes	Elements		Nodes	Depth (m)	
1			3	0.00	
4	1	20	6	0.25	
7	2	21	9	0.50	
10	3	22	12	0.75	
13	4	23	15	1.00	Sandy Loam
16	5	24	18	1.50	Sandy Soil
19	6	25	21	2.00	
22	7	26	24	2.50	
25	8	27	27	3.00	
	9	28			
28			30	5.00	
	10	29			
31			33	7.00	
	11	30			
34			36	9.00	
	12	31			
37			39	11.00	
	13	32			
40			42	13.00	
	14	33			
43			45	15.00	
	15	34			
46			48	17.00	
	16	35			
49			51	19.00	
	17	36			
52			54	21.00	
	18	37			
55			57	23.00	
	19	38			
58			60	25.00	

**Figure 5-2. Finite Element Method Development  
Soil Amendments**

or reversing the downward leaching of the contaminant into the deeper soils and ground water supplies.

Alfalfa will be utilized as the plant species of choice as it has well documented remedial properties, known parameters, and is easily managed by conventional agricultural equipment (Tracy et al. 1992, 1994, and Banwart et al. 1991). Figure 5-3 illustrates the changes in the spatial development from the addition of alfalfa to the test zone during the last test scenario 4.

Alfalfa's root density was approximated as being 0.080 in the first 0.25 meter, 0.071 from 0.25 m to 0.5 m, and 0.055 from 0.5 m to 0.75 m. Below 0.75 meters, the roots are not typically present in the soil. Therefore, the root density is set to zero for all depths below 0.75 m. This does not infer that the roots do not have an effect on the soil and soil-water below the 0.75 m depth.

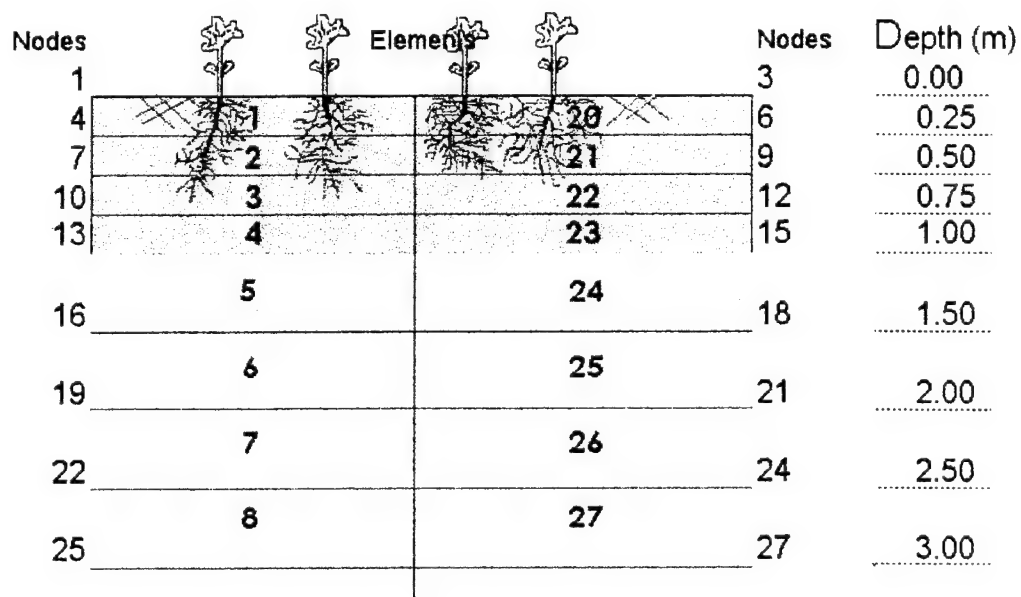


Figure 5-3. Finite Element Model Development,  
Establishment of Alfalfa Foot Zone.

## **CHAPTER 6.**

### **DISCUSSION OF RESULTS**

In order to analyze the output from the BIOROOT model, the concentration history and contour plot files for each simulation were imported into a spreadsheet and manipulated to produce the graphical results presented in this chapter. Simultaneous comparisons of the four scenarios were then possible.

For all the scenarios, the output was formatted to monitor the results of the pressure heads and contaminant concentrations at depths of 0.25, 0.5, 0.75, 1.00, 1.50, 2.00, 2.50, and 3.00 meters. Figures 6-1 through 6-10 track the variations of the TNT concentration as a function of both time and increasing depth. The model can also track the mass flux and the cumulative mass of the contaminant passing an arbitrary boundary condition. This boundary was set at a depth of 3.0 meters. Water fluxes through the zone of interest are from storm event infiltration, evaporation, and plant root transpiration. Figures 6-11 and 6-12 monitor the mass flux and the accumulating mass of system.

Significant contaminant concentrations were not observed at depths greater than 3.0 meters, therefore, summary figures do not indicate depths greater than 3.0 meters. The response of the various scenarios are compiled on the concentration profile figures at specific time intervals and depths. These profiles provide a "snapshot" summary of the contaminant's behavior as it moved through the area of interest.

***TNT CONCENTRATION VERSUS DEPTH PROFILES.***

Examining the "No Degradation" responses in Figures 6-1 through 6-5, a noticeably higher concentration profile exists that is greater than the other scenario profiles. During the first year the advective-dispersive processes dispersed the TNT resulting in a decrease of 63% of the material leaching from the 0.25 m depth. The initial 1400 mg/l TNT contamination in the upper soil regions decreased to 600 mg/l (0.25 m depth) and dispersed to a concentration of approximately 50 mg/l at the 3 meter depth. Subsequent time steps show the concentration curves flattening and dispersing the contaminant by approximately 24% (0.25m depth). Although not plotted, the concentration after 11 years was estimated to range from 199 mg/l at 0.25 meters to 166 mg/l at 3.0 meters. The last three years of the simulation resulted in dispersing only 10% of the remaining TNT from the 0.25 meter depth.

The other test scenarios, all of which involve a decay term, demonstrate that degradation has a significant influence on reducing the overall contamination level in the soil profile. When comparing the 1 year half life to No Degradation scenario, the only difference between the two scenarios is that the 1 year half life has implemented a decay rate at which one half of the contaminant will decay in one year. The difference in concentration between the two curves represent the amount of TNT that has decomposed or broken down



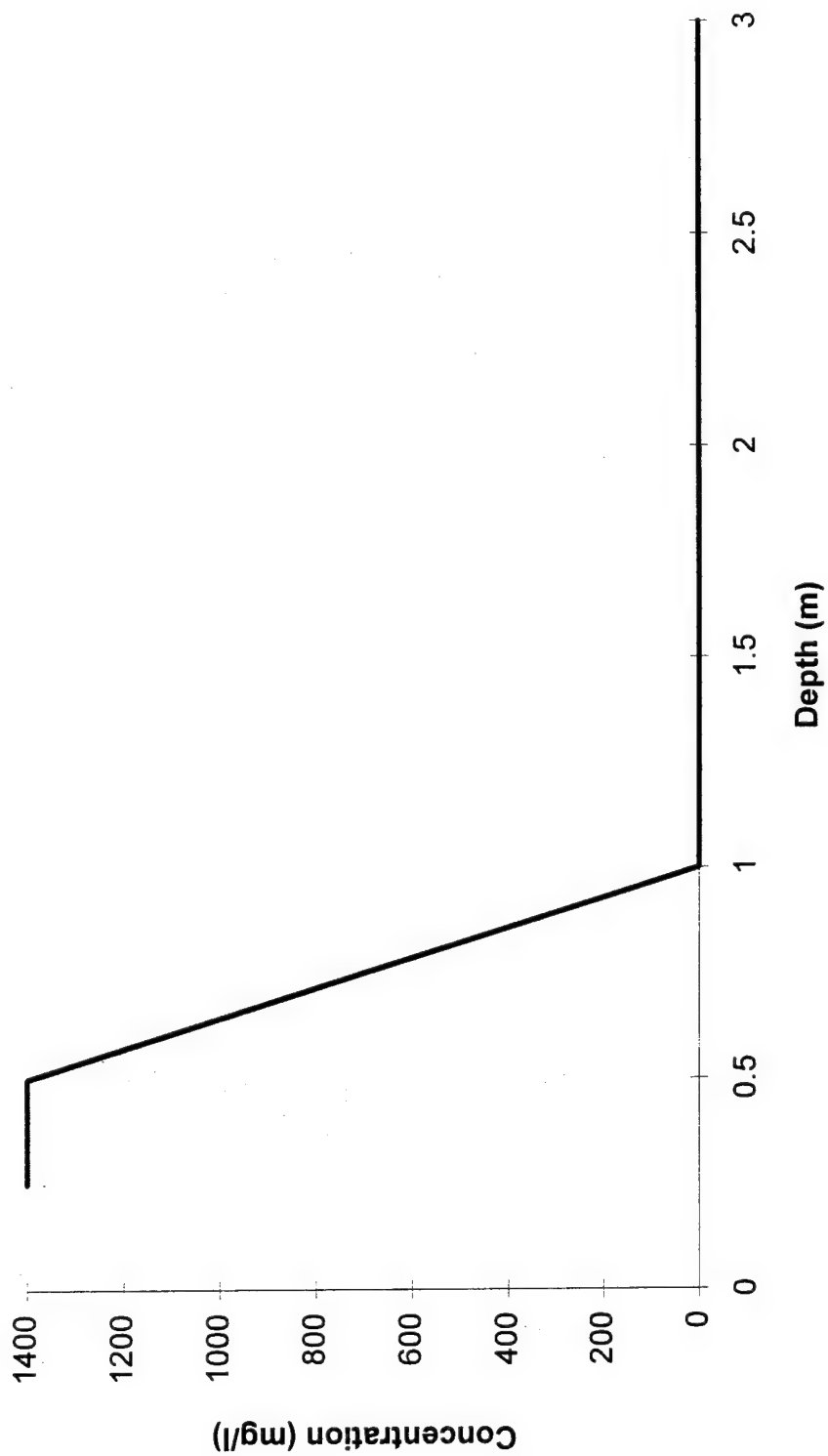


Figure 6-1. Initial Concentration vs Depth Profile  
Day 0

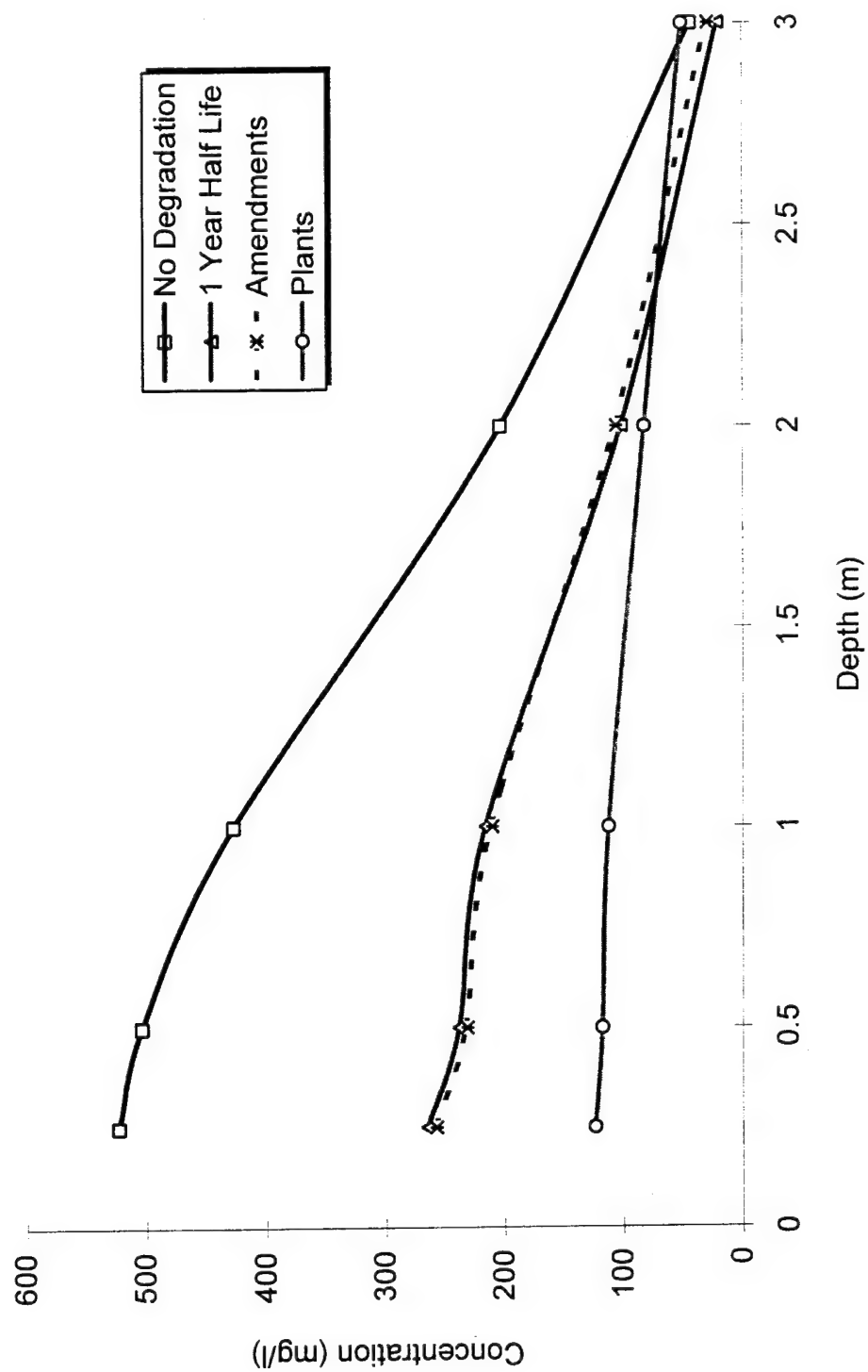


Figure 6-2. Concentration vs Depth Profile  
Day 366

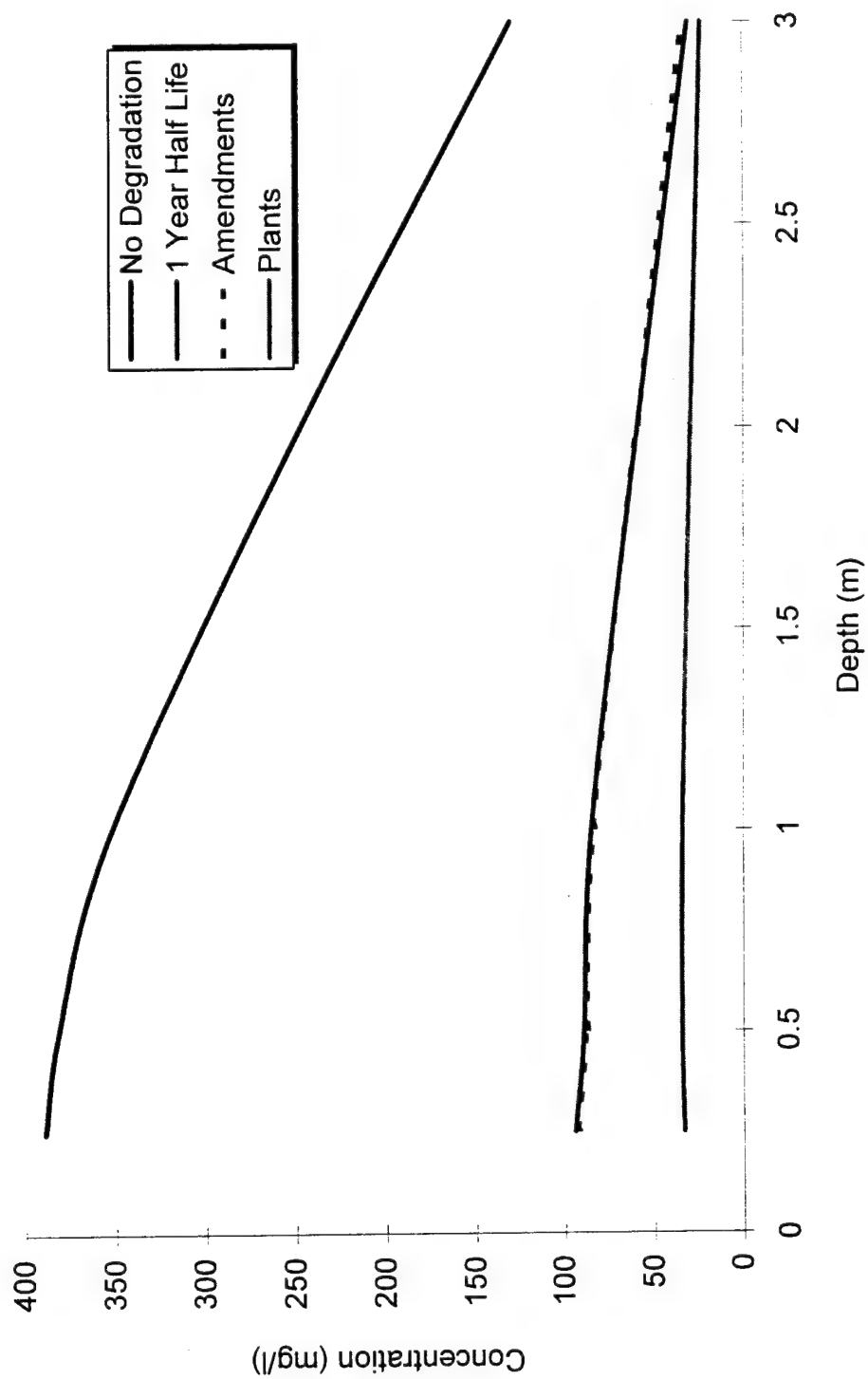


Figure 6-3. Concentration vs Depth Profile  
Day 731

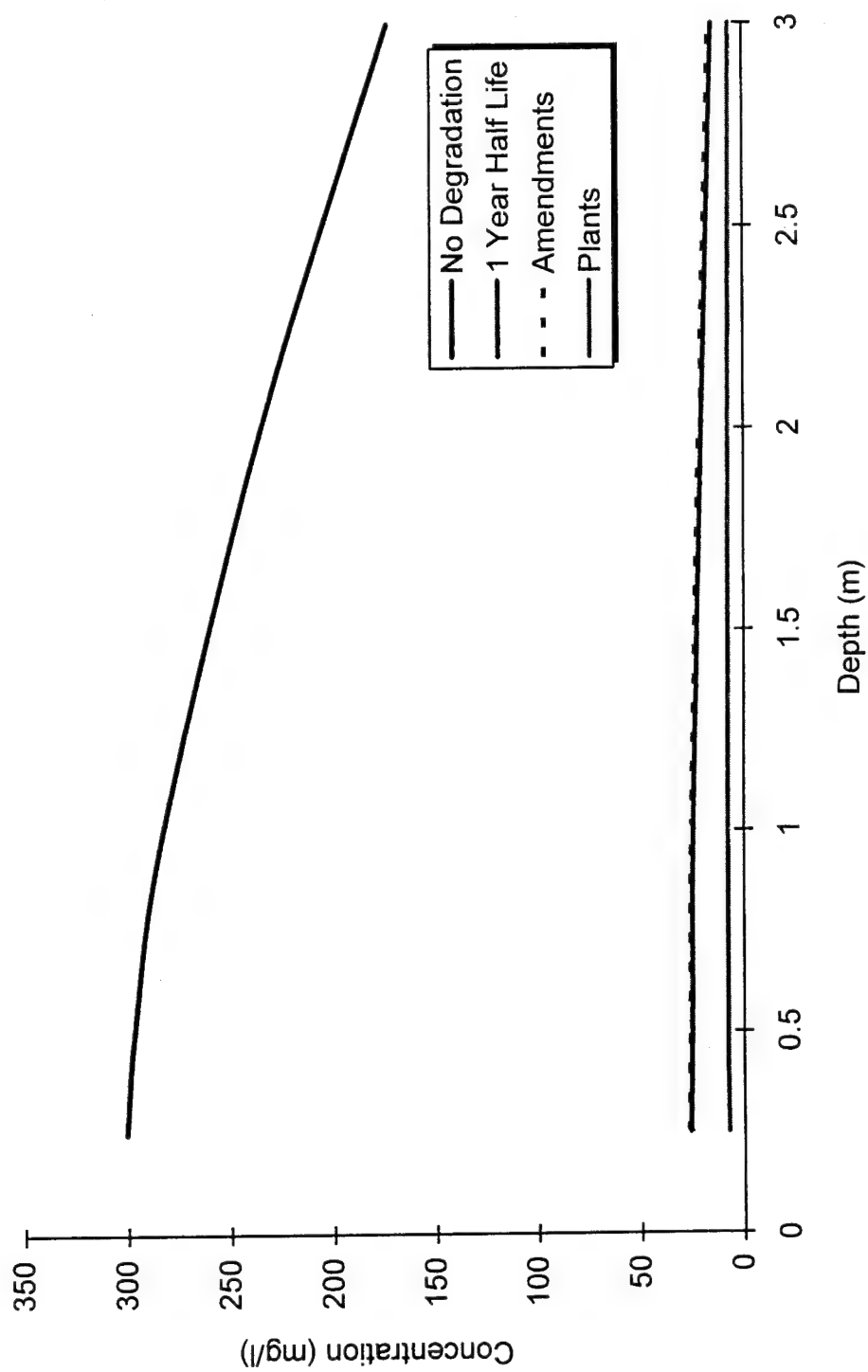


Figure 6-4. Concentration vs Depth Profile  
Day 1308

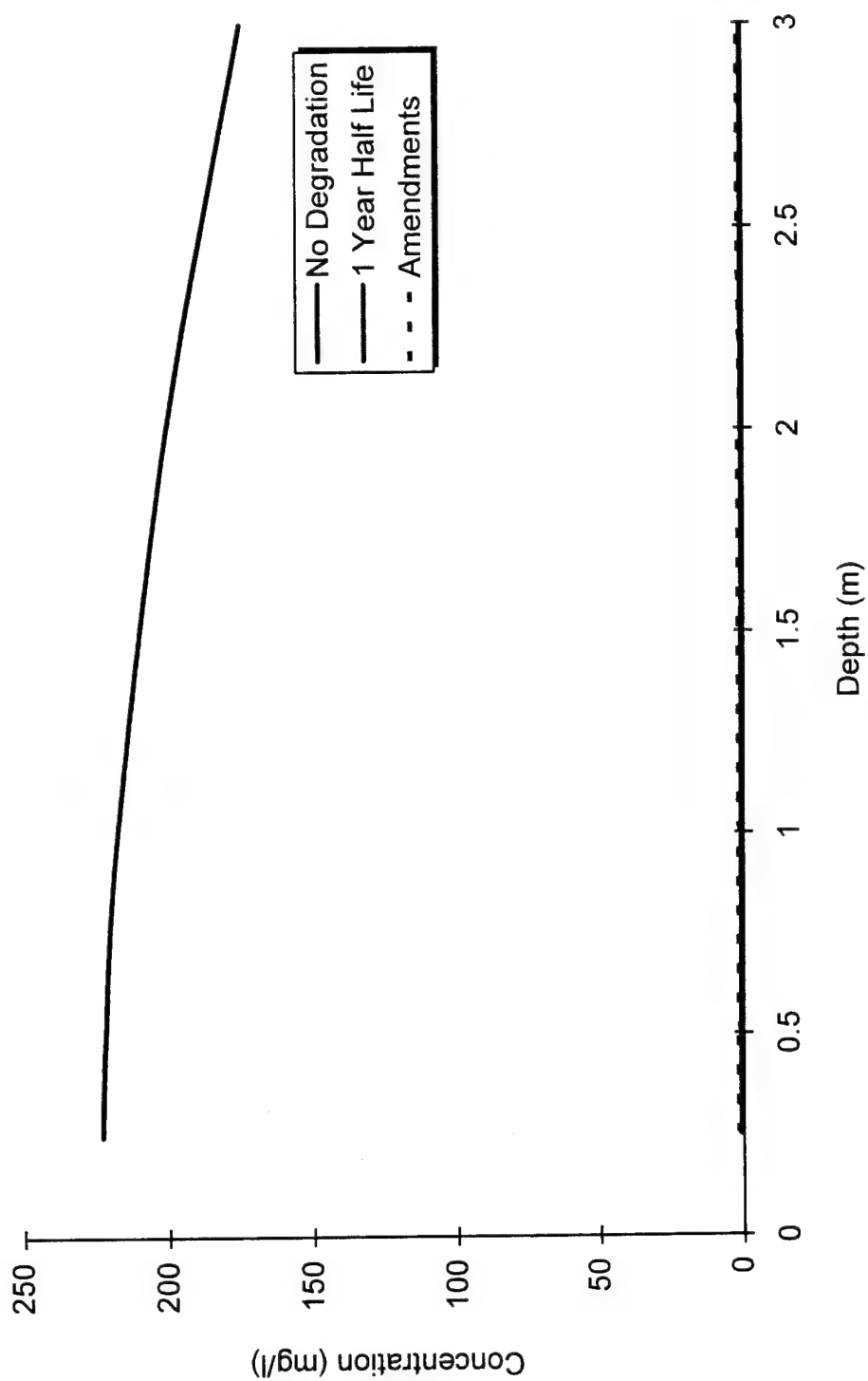


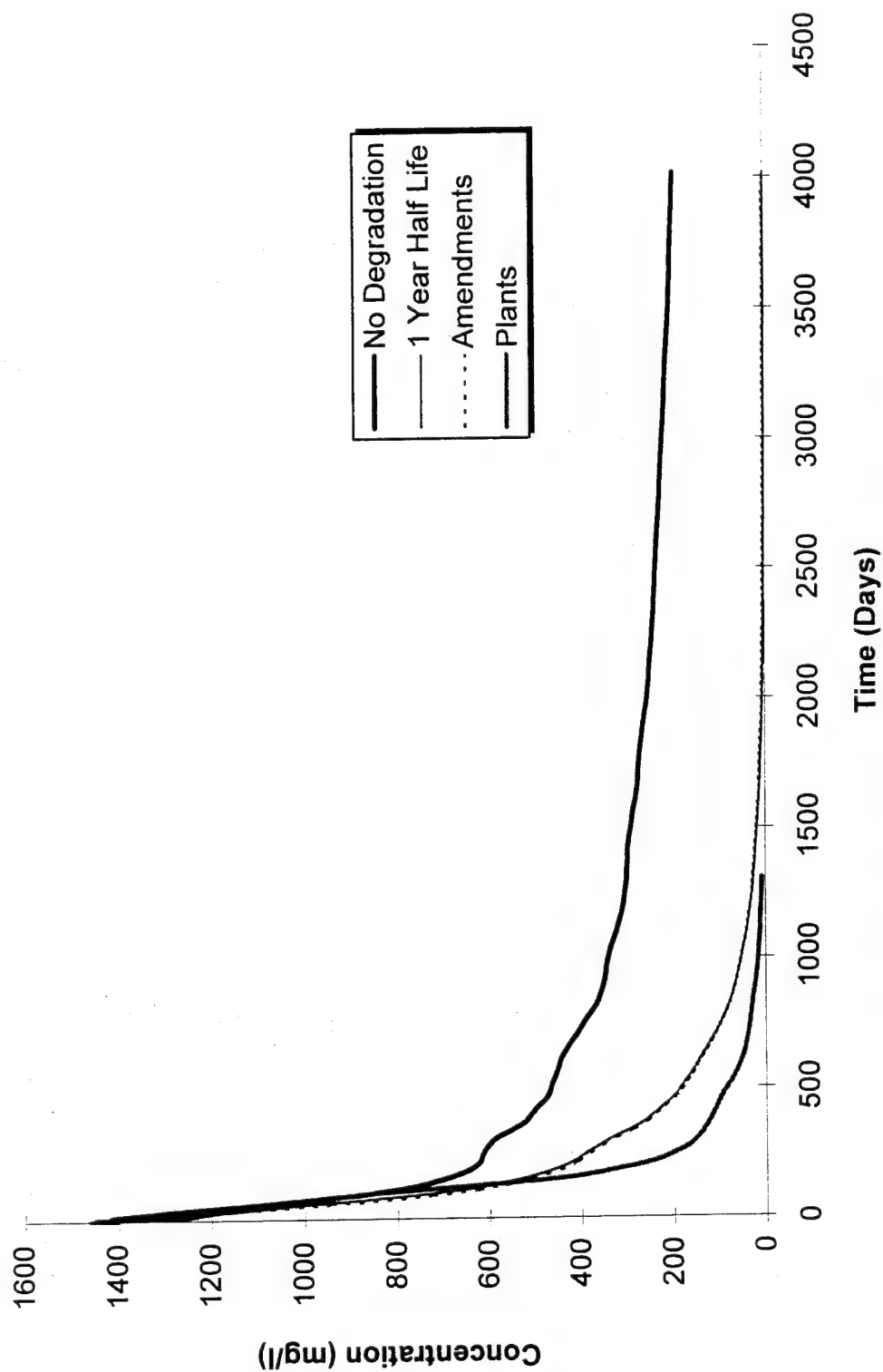
Figure 6-5. Concentration vs Depth Profile  
Day 2922

through the nitro reduction or methyl oxidation processes described in the literature review in chapter 2.

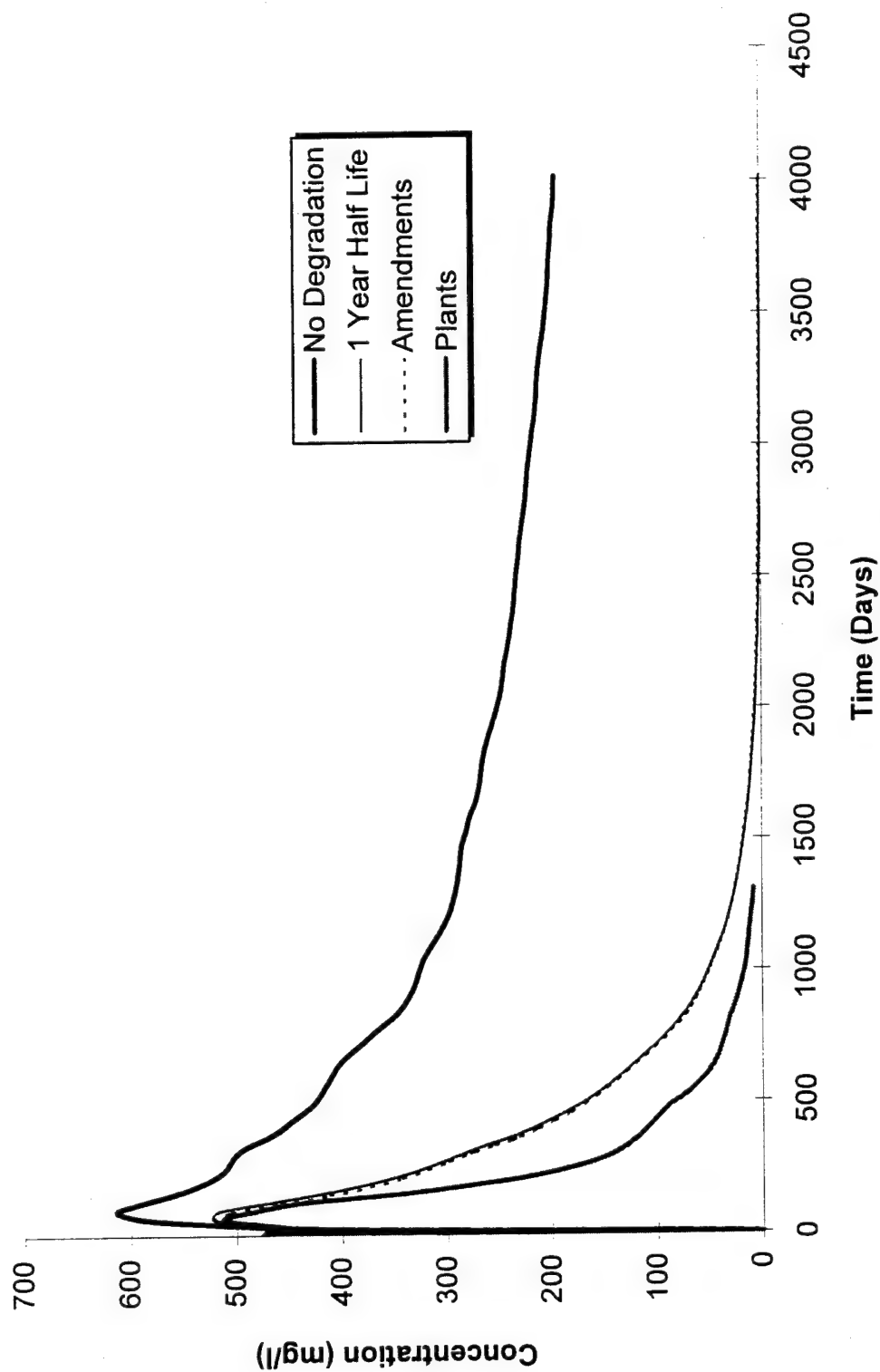
In all the figures presented in this chapter, the impact of amending the soil with 10% organic material offers minimal additional benefit as a stand alone remediation process when compared to the natural degradation of the contaminant. At no time did the amendments contribute significant degradation of the contaminant. Early in the simulations the amendments did decrease TNT concentration leaching to deeper soils. Thus, the amendments were able to retain more of the contaminant in the upper regions of the soil profile thereby making them available for capture by the plant system or natural degradation according to the contaminants half-life value. Amendments are a vital and mandatory step in preparing the site for vegetative remediation processes. This simulation verified the benefits of vegetative remediation were indeed from the alfalfa's uptake of the contaminant and not significantly from the additional adsorption sites provided from the amendments.

#### ***TNT CONCENTRATION VERSUS TIME PROFILES.***

These same relationships can be shown in the Concentration vs. Time profiles. Figures 6-6 through 6-10 also illustrate the advective dispersive relationships with respect to time and depth. Here the depth is held constant so that observations can be made with respect to the time variable. Comparing the responses between initial depths, 0.25 and 0.75 meters, the first observations

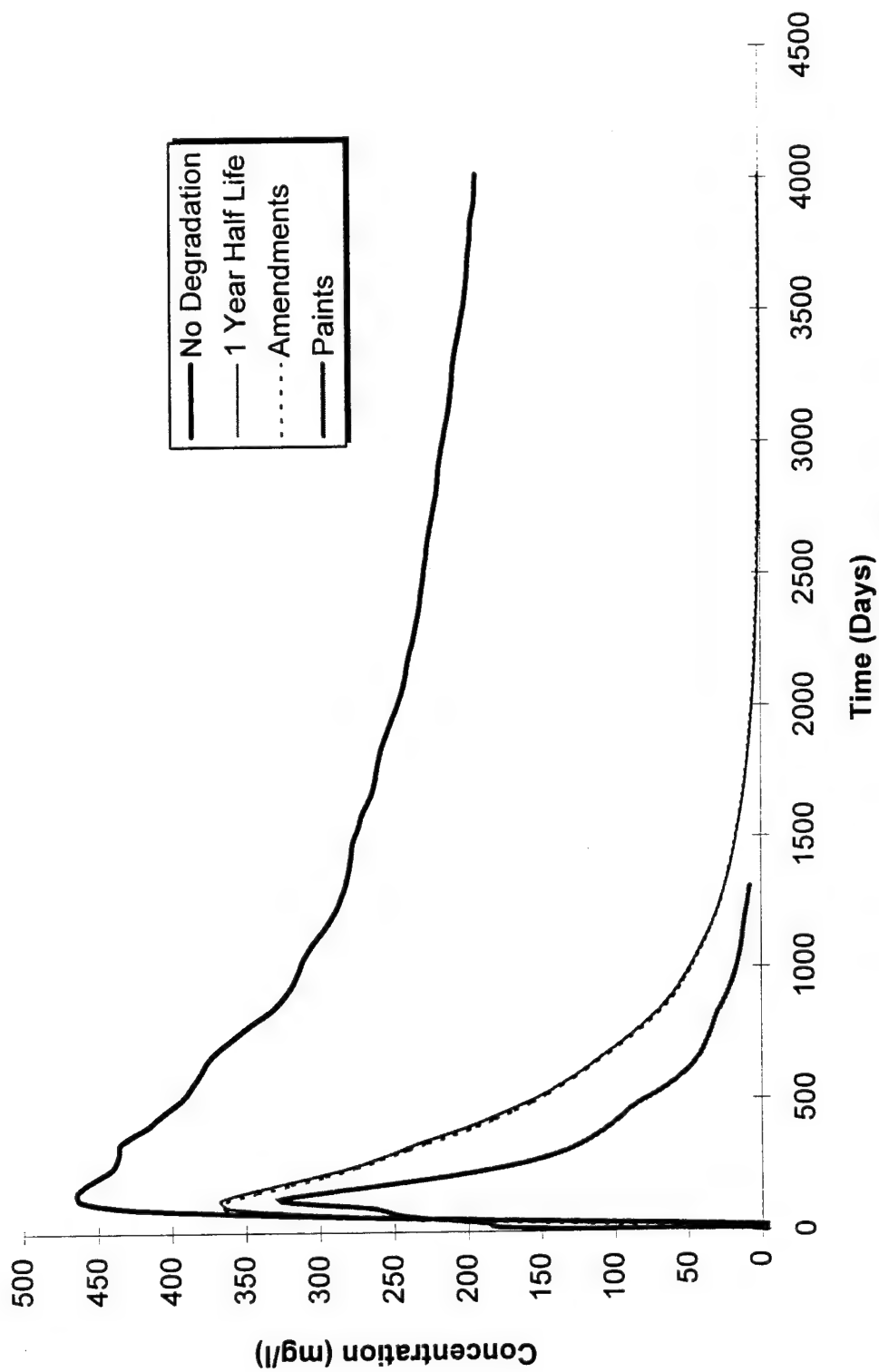


**Figure 6-6 Concentration Profile vs Time**  
0.25 m depth

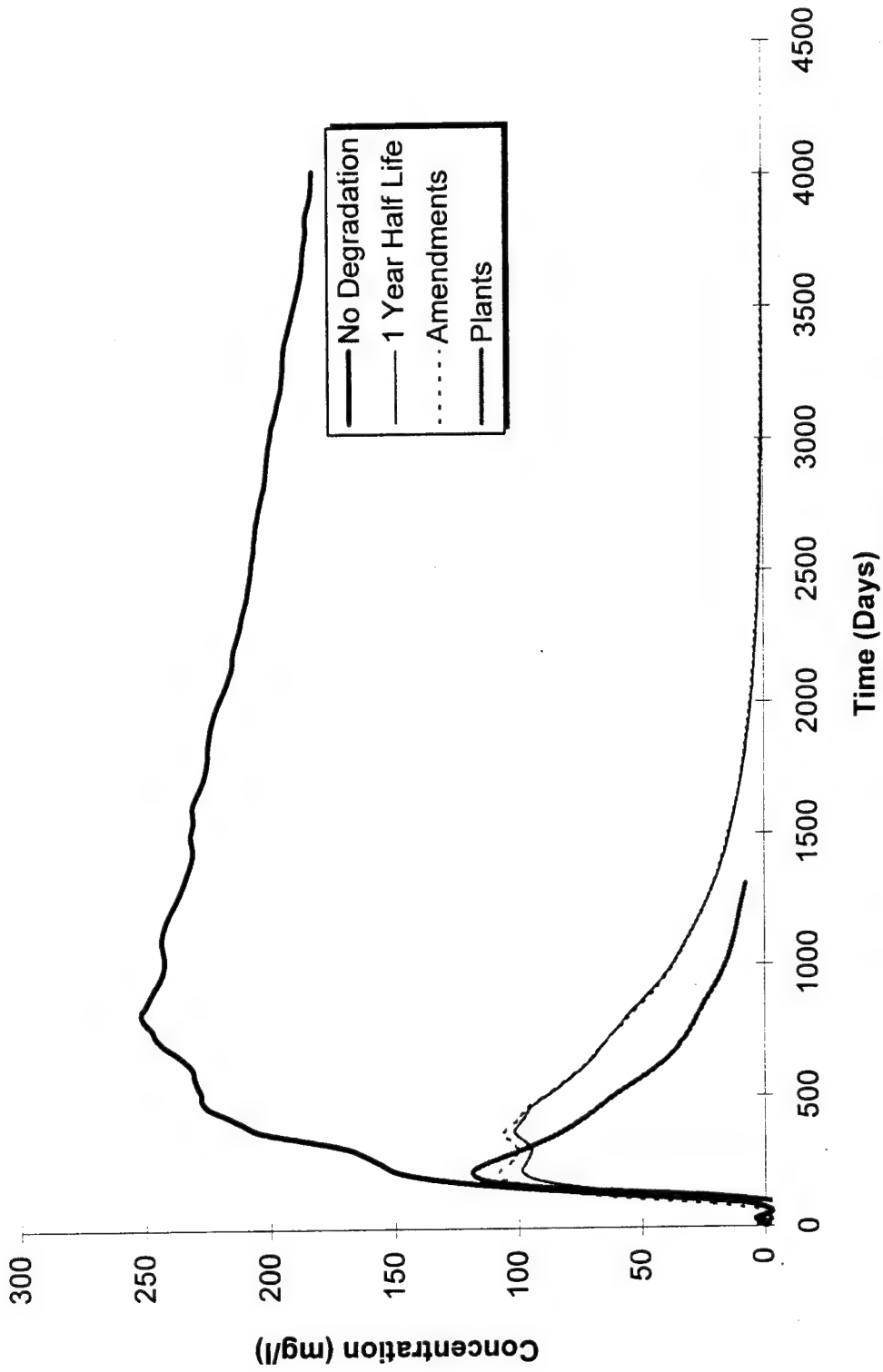


**Figure 6-7 Concentration Profile vs Time**  
**0.75 m depth**

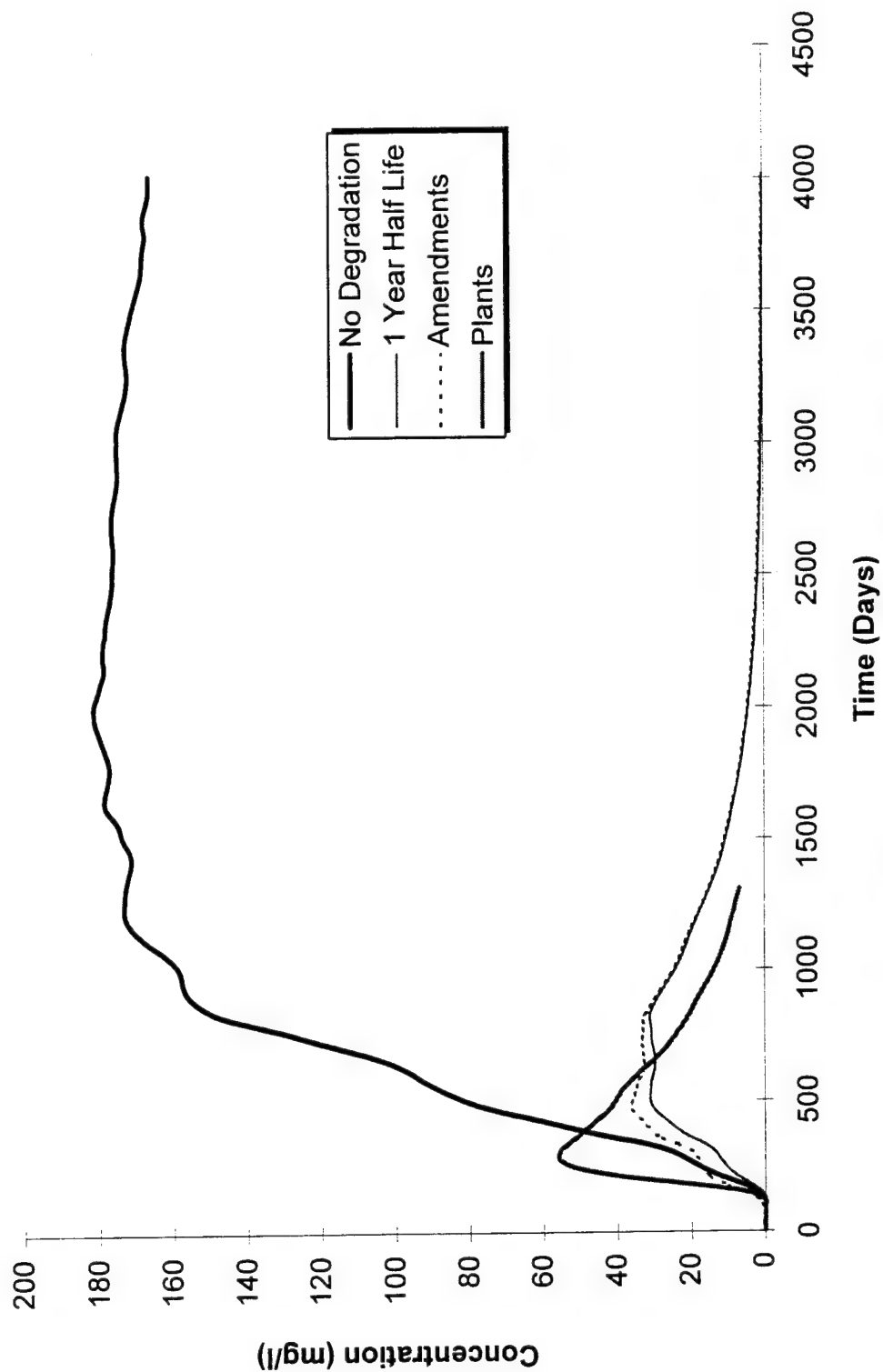




**Figure 6-8 Concentration Profile vs Time**  
**1.0 m depth**



**Figure 6-9 Concentration Profile vs Time**  
**2.0 m depth**



**Figure 6-10 Concentration Profile vs Time**  
**3.0 m depth**

concerning the downward movement of the TNT can be made. As TNT reached the 0.75 m depth, the observed concentrations reached a peak of about 620 mg/l and then immediately began to taper off. The initial sharp rise is the result of the initial wave of contaminant moving through the soil from time period 0. This same wave is also seen in all the remaining profiles, however the concentration intensity is reduced. This reduction is caused by 2 major factors: advection - dispersion transport spreading the plume downward and the adsorption interactions occurring with the clean soil. If the TNT contamination had responded as a plug flow contaminant, a very discernible wall effect would have been observed. Additionally, after the slug of TNT had passed, the concentration remaining in the soil could be attributed to the adsorbed phase.

The introduction of alfalfa plants into the study further decreases the concentration intensity of the plume. This can be attributed to not only the roots ability to capture TNT from the soil water phase but also the roots provide additional adsorption sites onto the root's structure.

An anomaly occurred in Figure 6-10 where the plant's curve is initially steeper than the No Degradation simulation. This indicates that the plants are causing the TNT to transport faster than the No Degradation response. There appears to be no viable reason for this to occur. Plant - contaminant interactions normally slow rather than accelerate the transport of the contaminant.

***MASS FLUX OF TNT.***

The BIOROOT model is capable of tracking the mass flux of the contaminant as it passes between two elements. In this study, mass flux was calculated at the lower boundary at a depth of 3.0 meters. The mass flux response is graphed with respect to time and is illustrated in Figure 6-11. All four scenarios exhibit a lag time of approximately 20 days which represents the amount of time required for the TNT to reach the 3.0 meter depth via advection and dispersion. The mass flux for the four scenarios are shown in Figure 6-10.

After the initial lag phase passed, the mass flux varies greatly between the different scenarios. The No Degradation response is highly erratic in its pattern. This can be attributed to a direct relationship with storm events and the amount of infiltration that is carrying the contaminant deeper into the underlying soil. The first major peak (4 mg/l, ~500 days) is the initial "breakthrough" of the TNT as adsorption sites in the upper soil regions are being exhausted. Breakthrough is a very common response with adsorption processes in traditional industrial wastewater treatment. Subsequent TNT mass fluxes continue to contribute to loading the adsorption sites within the soil matrix until complete exhaustion occurs. Adsorptive exhaustion is when the soil can no longer attract a meaningful concentration of contaminant solute from the soil-water phase onto the solid phase of the soil. This adsorption process can be described best by Figure 6-12 (Benefield et al. 1982) of an idealized carbon adsorption column

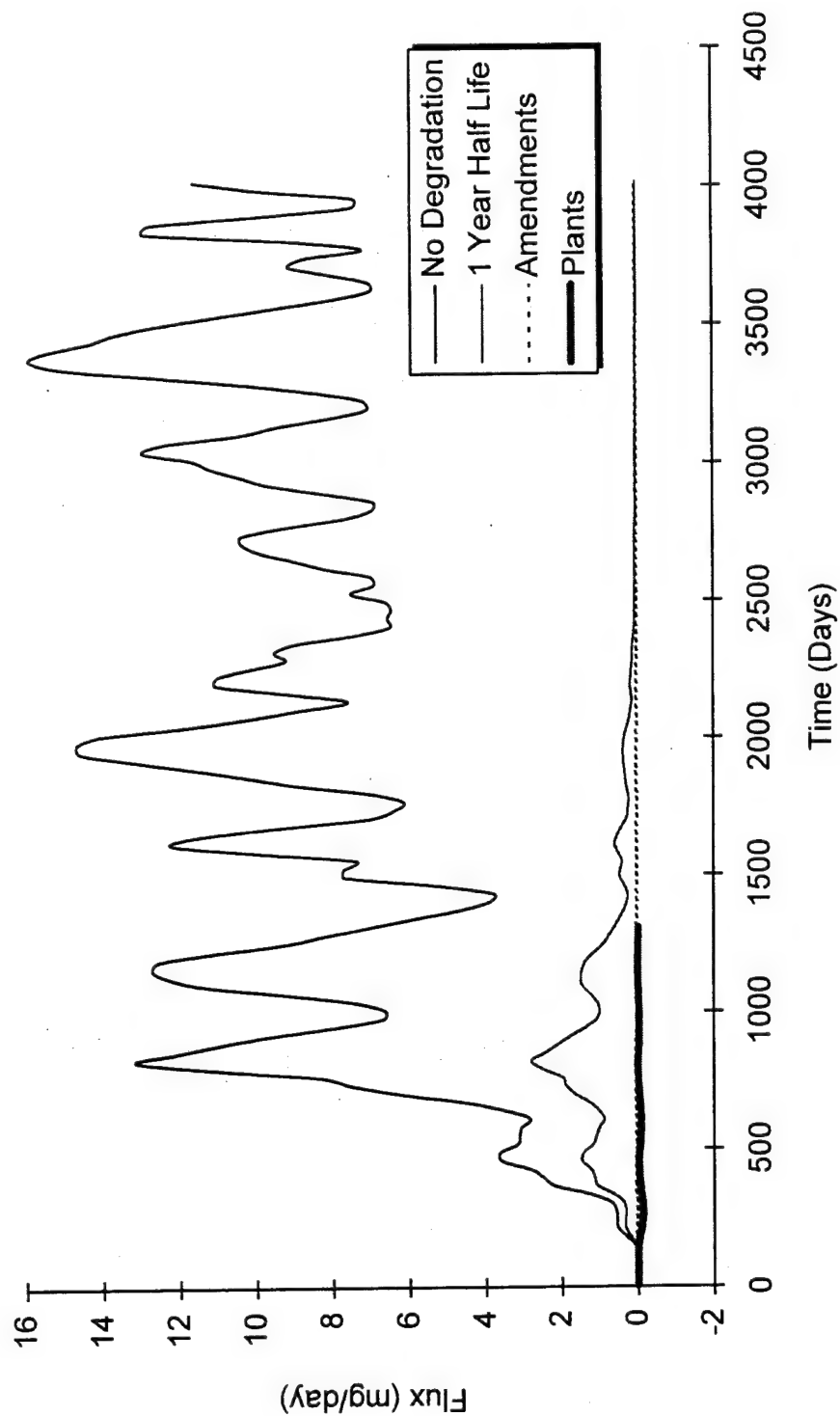
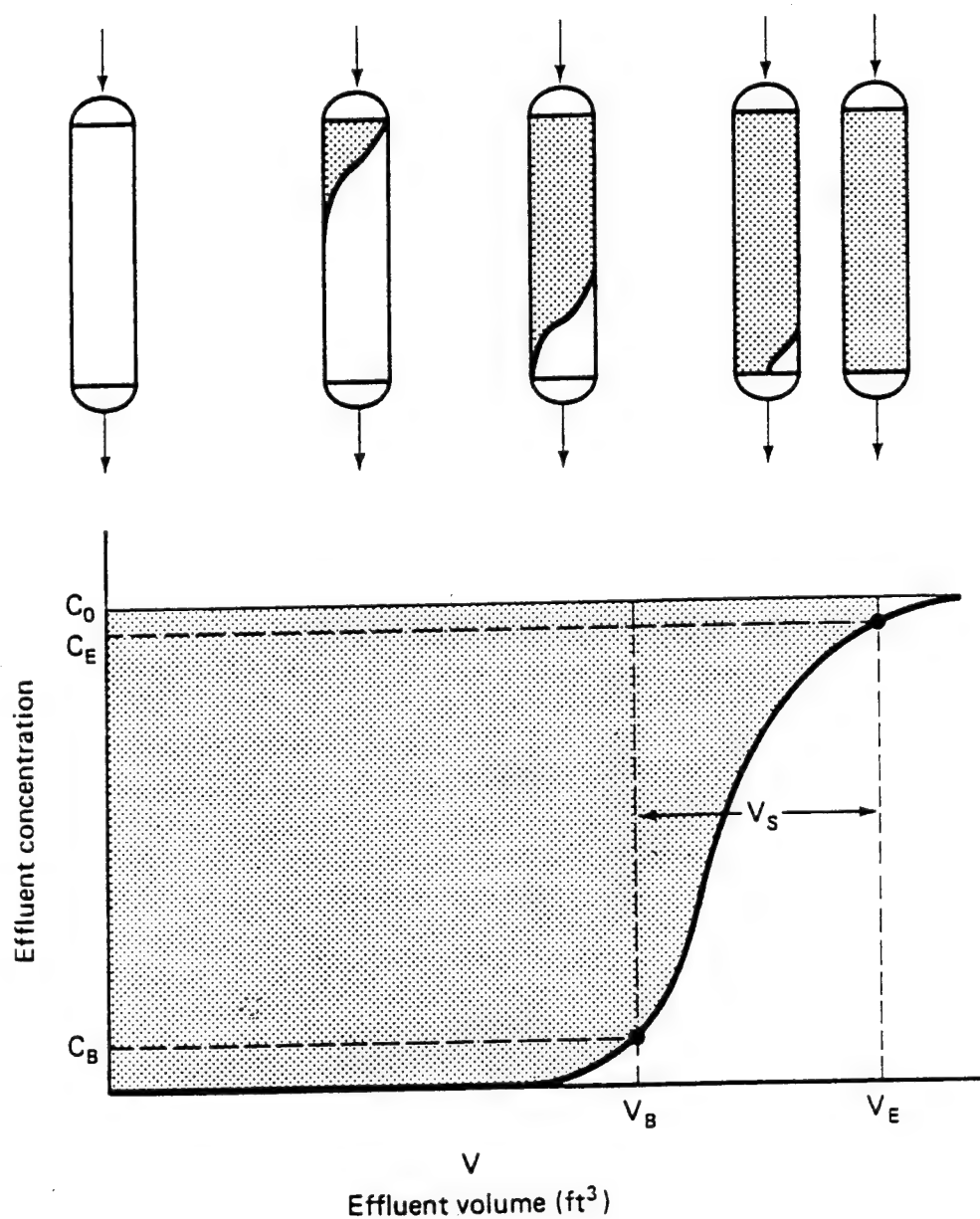


Figure 6-11. Mass Flux of the System at 3.0 m



**Figure 6-12. Idealized Breakthrough Curve for Carbon Adsorption (Benefield et al. 1982)**

undergoing normal loading of a compound. Benefield's column illustration simplifies the adsorption process occurring in the model of the UMDA site. Initially, the deeper soils are uncontaminated and will behave as the first column depicts. As TNT continues to leach into the soil, the TNT will adsorb to organic matter within the soil matrix. The third column illustrates breakthrough of the lower region of the column in the same manner that Figure 6-10 profile indicated. The fifth column graphically shows the column after the media has been completely exhausted and becomes unreactive in adsorbing additional contaminant.

After breakthrough and exhaustion have occurred, the compound will continue to pass through the media as a function of the annual precipitation cycle with little interaction or degradation. The upward slopes (toward the peaks) represent when storm events recharge the soil water and increase the soil water pressure head of the upper soil zones thus moving water and TNT downward. The downward slopes represent the drought cycle when storm events are not contributing significant quantities of water, thus decreasing the upper soil water pressure head on the system. Therefore, the "No Degradation" scenario exhibits classic advective - dispersive behavior as a conservative contaminant after breakthrough has occurred.

The other scenarios exhibit similar responses except for the fact that their respective degradation factors are eliminating TNT from the total mass of the system. The mass flux in the vegetation scenario is negative. This indicates that



the root zone is capable of extracting TNT from below the 3.0 meter depth. Although the roots are physically located in the top 0.75 meter of soil. They transport water from soil depths below 0.75 meters. Thus, the roots are behaving as a contaminant sink, drawing the contaminant toward the roots and internalizing the TNT.

#### ***TOTAL TNT MASS LEACHING FROM SOIL.***

The cumulative mass of TNT passing through the 3.0 m depth is also monitored by the BIOROOT model. By monitoring the total mass of TNT that has passed through a specific depth profile, a true picture of the fate and transport of the contaminant can be understood. Figure 6-13 illustrates the cumulative mass leaching into the deeper soil profiles and possibly the ground water. The "No Degradation" scenario has contributed over 7000 grams of TNT per square (surface) meter to the soils deeper than 3.0 meters. The 1 year half life simulation contributed almost 1000 g, the amendments only 21 g, and the plants were capable of reversing the contaminant migration by removing 49 g from the deeper soils.

The effects of incorporating vegetative remediation technologies is well illustrated in Figure 6-11. In this study the root system was located in the top 0.75 meter but was able to influence and draw up TNT from depths greater than 3.0 meters. This implies that the roots have a capability of influencing contaminant migration toward the root zone up to 3x the actual distance from the

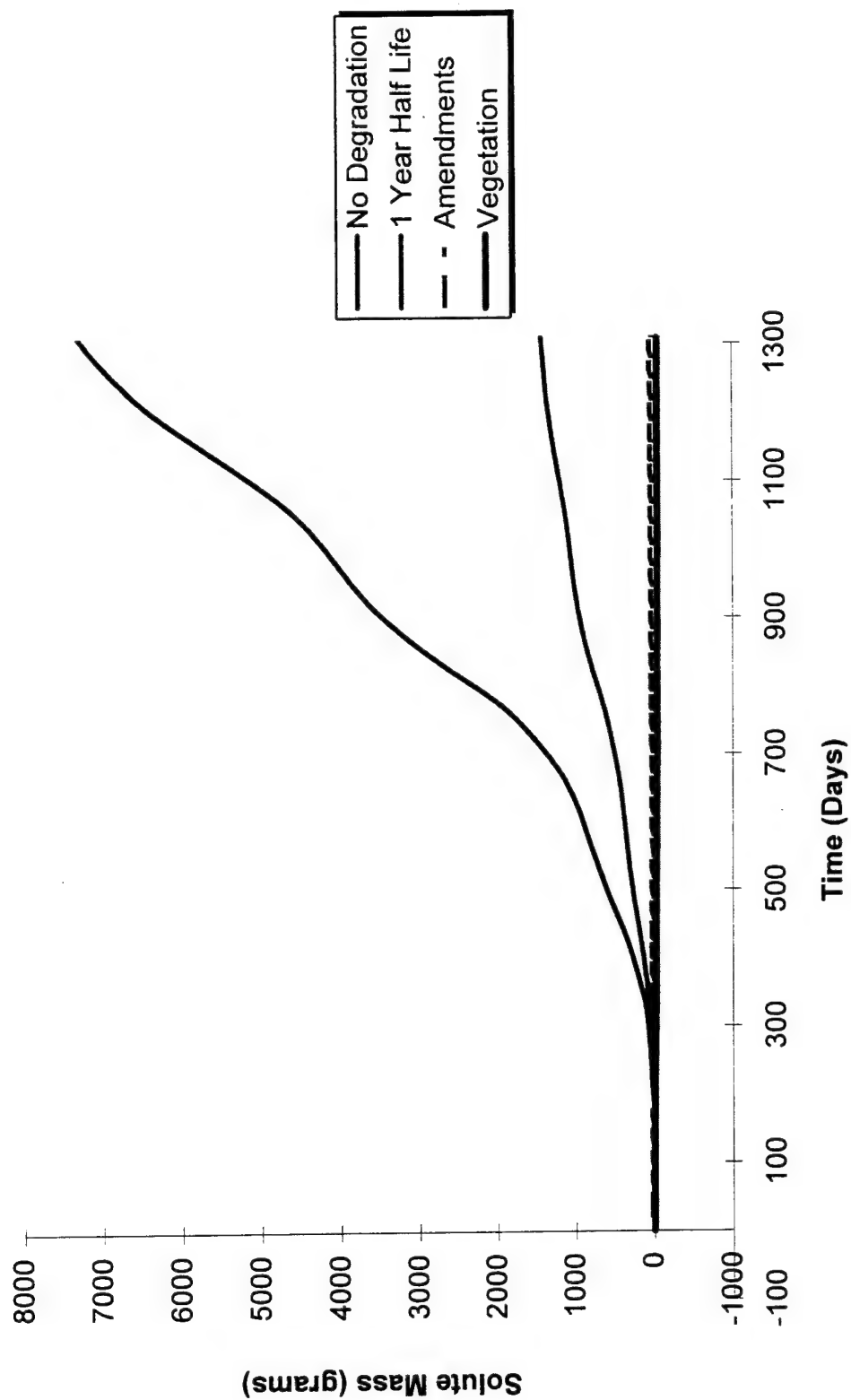


Figure 6-13. Total Mass of TNT Leaching through 3.0 m

root zone. Vegetation is capable of removing contaminants from distances greater than the physical location of the root system and contain the TNT contaminant "in place" by not allowing further migration and pollution of the underlying soils and ground water sources.

## **CHAPTER 7.**

### **CONCLUSIONS**

The BIOROOT model simulates the fate and transport of contaminants through variably saturated soil conditions exceptionally well. This model behaved according to known field, laboratory, and textbook adsorption concepts. The responsiveness of the No Degradation mass flux scenario indicate that the model responded well to the minor infiltration fluxes associated with the arid climate of the Umatilla Depot Activity and the surrounding Hermiston, Oregon area.

The surface contamination of the explosive washout lagoons at the Umatilla Depot Activity near Hermiston, Oregon may not require expensive ex-situ remediation and restoration processes. The continued migration of the explosive contaminants into the ground water may not only be halted but may also be extracted from the soil matrix and remediated by plants. The use of vegetative remediation in this study indicate that the root system's area of influence may be capable of removing contaminants beyond their physical reach. Additional research applying both vegetative remediation and field application in situ modeling, as a daily monitoring tool, in pilot scale and then field demonstration experiments may be warranted based on this research.

The majority of the recent research has been toward identifying microbial populations, such as the white rot fungus and various psuedomonas organisms, capable of in situ remediation of explosive compounds. Little research has focused on vegetation processes other than top soil erosion control. The ability of vegetation to flourish in contaminated environments and metabolize the contaminant may provide more remedial capability and capacity than thought before. Other plant species, such as the wild tomato or fescue and rye grasses may be more tolerant of explosives compounds in this study, which may not require expensive soil amendments or other augmentative precursors. However, the cost of amending the soil with 10% organic material is still less costly than the operating costs associated with pump and treat or other ex situ remediation processes.

The BIOROOT model requires that a complete and thorough understanding of the targeted remediation site be known. The input parameters to this model require exceptional skill in determining valid parameter inputs versus field measured values that are commonly accepted but may not be valid in the circumstances simulated. For instance the range of the hydraulic conductivity for the UMDA site are reported as being large (277 ft/day) to very large (3270 feet/day, ESE 1991). The problem stems from the application of the traditional saturated soil values versus the relative values commonly associated with non-isotropic, non-homogeneous variably saturated conditions. Proper

model calibration is necessary to account for site specific heterogeneity when applying the model to an actual site during hypothetical remediation operations.

BIOROOT was able to predict and illustrate the relative efficiencies associated with alternative remediation processes. The incorporation of vegetative remediation techniques are favorable for TNT contamination and should be sought out and exploited. Results from this research could be applied to determine the cumulative remedial effects of these same processes and provide an updated estimation of the time necessary to remediate the site to an acceptable level.

The BIOROOT model is limited to simulating only one degradation process at a time. This might be overcome through the use of superposition techniques to establish a cumulative degradation factor that can be input into the model. Continued model development should incorporate simultaneous multiple degradation processes. The additional capability of expanding the model to address additional contaminants such as the generation and degradation of intermediate daughter products is warranted. A more complex representation of biological degradation would have been incorporated into this study had the model been able to incorporate multiple degradation reactions. This type of modeling would also require biological kinetic data which is not available at this point in time.

### ***RECOMMENDATIONS FOR FUTURE RESEARCH***

Additional research could be conducted to determine the modeling efficiencies of BIOROOT on remediating TNT contamination from saturated soils. This would involve establishing an in situ anaerobic biological system in the saturation region. The concentration of the contaminant in the soil-water must be below the threshold level of 200 ppm for biological activity to be initiated (Funk et al. 1993). TNT concentrations of 50 mg/g were reported at depths of 10 to 50 feet (water table). Soil water concentrations in the saturated region measured 50 mg/l. The biological species may be able to remediate munitions contaminating the variably saturated region immediately above the water table (Funk et al. 1993).

A sensitivity analysis should also be completed on the model to determine which parameters are more consequential. This study alone identified that the variation of the half life degradation factor had a significant impact on the overall remediation of the washout lagoons. The model's ability to monitor the mass flux of the system under arid climates indicates the responsiveness and sensitivity of the governing adsorption - dispersion equation. Other parametric variables may or may not have similar significant effects on the model. Those parameters that have pronounced effects on the model must be focused on in order to ensure accuracy and validity. Sensitivity analysis also provides a prioritized method for obtaining and utilizing parametric information. Environmental parameters of

major significance should be obtained from either laboratory, pilot, or field scale experiments or surveys. Priorities can be directed at those parameters and information that will yield the most results for the capital resources obligated. Parameters of minor significance may be estimated if necessary. The acquisition of non-significant parameters can be further prioritized without adversely affecting the validity of the results. All too often financial resources are limited and require responsible decisions to acquire not only the most information possible, but more importantly, the right information.



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**APPENDICES**

**APPENDIX A.****DEFINITIONS OF MODEL PARAMETERS**



### PARAMETER DEFINITIONS

An alphabetical listing of the parameters and their definitions is listed below.

$\eta$	soil porosity
$\theta$	soil-water content
$\beta$	storativity indicator. $\beta = 1$ if $\psi_s \geq 0$ , $\beta = 0$ if $\psi_s < 0$ .
$\rho_b$	bulk density of the soil
$\psi_r$	root water pressure head
$\psi_s$	soil water pressure head
A	soil characteristic parameters
c	soil characteristic parameters
C	solute concentration
$C_r$	contaminant concentration adsorped onto the root structure
$C_{ts}$	contaminant concentration in the plant's transpiration stream
D	Dispersion coefficient
k	first order decay rate
$k_1$	adsorption coefficient
$K_r$	hydraulic conductivity of the root
$K_s$	hydraulic conductivity of the soil
q	soil-water extraction rate by the plant's root system
$R_{cf}$	root concentration factor
S	contaminant sink due to plant uptake
$S_e$	effective saturation of the soil. $= \theta/n$
$S_s$	specific storage of the soil (storativity)
$S_y$	specific yield of the soil
t	time
$T_{scf}$	plant's transpiration stream concentration factor
V	Darcy soil-water flux
$WC_r$	root water content
x	horizontal spatial dimension
z	vertical spatial dimension

**APPENDIX B.**

**BIOROOT SIMULATIONS; HISTORY FILES**



## No Degradation

1186	12.5551	6207.936	-8.7151	309.6	-8.6247	306.1	-8.531	300.3	-8.4343	292.3	-8.2323	270.1	-8.0198	241.1	-7.7971	207.8	-7.5642	172.5
1216	11.1702	6543.041	-9.72	306.5	-9.5022	302.8	-9.2972	297	-9.1029	289.1	-8.7401	267.5	-8.4028	239.5	-8.0826	207.2	-7.7731	173.2
1247	9.3047	6831.487	-9.6843	304.2	-9.5231	300.3	-9.3607	294.4	-9.1979	286.5	-8.725	265.2	-8.3492	237.8	-8.2283	206	-7.9096	173.2
1277	8.2251	7078.239	-10.1212	302.2	-9.9172	298.4	-9.7187	292.4	-9.5249	284.6	-9.1493	263.5	-8.7864	236.4	-8.4328	205.3	-8.086	173.1
1308	7.0454	7296.646	-10.4139	300.6	-10.2039	296.7	-9.9978	290.6	-9.7952	282.7	-9.3997	261.8	-9.0153	235.1	-8.6401	204.4	-8.272	172.9
1339	5.8509	7478.023	-10.8567	298.5	-10.6176	295.3	-10.385	289.1	-10.1581	281.2	-9.7194	260.3	-9.2978	232.8	-9.1128	202.4	-8.4924	172.5
1369	4.7208	7619.647	-11.1477	296.8	-10.9051	294.4	-10.6873	288	-10.434	280	-9.9796	259.1	-9.5399	232.8	-8.8997	203.4	-8.696	172
1400	3.88	7739.926	-11.3858	298.2	-11.1418	293.6	-10.9016	287	-10.6651	279.1	-10.2024	258.1	-9.752	231.8	-9.3125	201.5	-8.8822	171.5
1430	3.7543	7852.557	-11.118	297.5	-10.9324	292.9	-10.7422	286.5	-10.5483	278.4	-10.1525	257.4	-9.7498	231.2	-9.3435	201.2	-8.9356	171.3
1461	5.3883	8019.594	-10.0045	294.7	-9.849	291.4	-9.6759	285.7	-9.4871	277.9	-9.5694	257.3	-9.3086	231.4	-9.0144	202.2	-8.6947	171.9
1492	7.6843	8257.809	-9.7482	291.4	-9.6599	288.6	-9.5661	283.7	-9.4665	276.6	-9.2489	257	-9.0068	232	-8.7414	203.7	-8.4545	173.3
1521	7.8953	8480.972	-10.623	289.3	-10.3977	286.2	-10.1845	281.3	-9.981	274.5	-9.5959	255.7	-9.2302	231.5	-8.875	203.8	-8.5239	174.1
1552	7.3676	8709.367	-9.8784	287.2	-9.7834	284.2	-9.6769	279.4	-9.5606	272.7	-9.3044	254.5	-9.024	230.8	-8.7252	203.7	-8.4119	174.7
1582	10.0264	9010.158	-8.4621	283.9	-8.4969	281.6	-8.5114	277.3	-8.507	271.2	-8.4479	253.9	-8.3312	231.2	-8.1666	205	-7.9624	176.1
1613	12.2262	9389.171	-9.0107	280.5	-8.8947	278.2	-8.7838	274.3	-8.6761	268.7	-8.4642	252.6	-8.2497	230	-8.0913	205.6	-7.8107	178.6
1643	11.4617	9733.021	-9.3869	277.9	-9.233	275.5	-9.0631	271.5	-8.9364	266	-8.6504	250.6	-8.3701	230	-8.0913	205.6	-7.8107	178.6
1674	9.3384	10000.000	-10.1715	276.2	-9.9416	273.6	-9.722	269.4	-9.5114	263.9	-9.1128	248.7	-8.7374	228.5	-8.3785	204.4	-8.0309	178.4
1705	6.982	102607.000	-10.6207	275.2	-10.3814	272.3	-10.1488	267.9	-9.9224	262.4	-9.4867	247.1	-9.0705	227.1	-8.6701	203.1	-8.2823	177.8
1735	6.367	105000.000	-10.1358	274.2	-9.9939	271.4	-9.8441	267	-9.6878	261.4	-9.3606	246.1	-9.0199	225.5	-8.6615	202.1	-8.4732	177.2
1766	6.1318	10766.000	-10.765	273	-10.5307	270.3	-10.3048	266	-10.0856	260.4	-9.6635	245.2	-9.2571	225.5	-8.6615	202.1	-8.4732	177.2
1796	7.0499	110333.000	-9.4007	271.2	-9.3675	268.9	-9.3133	265	-9.241	259.5	-9.0321	244.6	-8.8172	225.1	-8.5482	202.2	-8.2539	177.4
1827	8.94	113000.000	-9.5956	269.1	-9.4697	267	-9.3445	263.5	-9.2187	258.4	-8.9624	244	-8.6962	225.1	-8.4179	202.8	-8.1266	178.1
1858	10.3146	11566.000	-8.8915	266.7	-8.842	264.7	-8.7817	261.4	-8.7116	256.6	-8.5452	242.9	-8.3485	224.7	-8.1257	203.1	-7.8902	178.9
1886	11.6117	118321.000	-8.9321	264.5	-8.8358	262.7	-8.7383	259.5	-8.639	254.9	-8.4329	241.8	-8.2147	224.3	-7.9827	203.3	-7.7361	179.6
1917	13.245	121000.000	-8.047	261.9	-8.0382	260.2	-8.0171	257.2	-7.9848	252.8	-7.8895	240.5	-7.7585	223.7	-7.5964	203.5	-7.4071	180.4
1947	14.5806	123666.000	-8.3593	259.4	-8.2819	257.7	-8.1669	254.9	-8.0731	250.8	-7.8853	239	-7.6927	222.9	-7.4914	203.5	-7.2787	181.1
1978	14.6687	126333.000	-8.1557	256.9	-8.0824	255.2	-8.0053	252.4	-7.9244	248.5	-7.7525	237.2	-7.5874	221.8	-7.3696	203	-7.159	181.4
2008	14.0941	129000.000	-8.6159	254.8	-8.4767	253.2	-8.342	250.4	-8.2107	246.5	-7.9555	235.5	-7.7061	220.5	-7.4583	202.2	-7.2091	181.4
2039	11.9333	131666.000	-9.3344	253.2	-9.1328	251.3	-8.9397	248.4	-8.754	244.8	-8.4017	233.7	-8.069	219	-7.7504	201	-7.4414	180.8
2070	10.2584	134333.000	-9.2622	251.8	-9.1118	250	-8.9595	247	-8.8061	243.1	-8.4971	232.3	-8.1874	217.7	-7.878	199.9	-7.569	180.1
2100	8.9077	137000.000	-10.0035	250.8	-9.7713	248.8	-9.549	245.8	-9.3352	241.9	-8.9286	231.1	-8.5441	216.6	-8.176	198.9	-7.8197	179.5
2131	7.5716	139666.000	-10.0096	248.8	-9.8228	247.8	-9.6359	244.7	-9.4492	240.8	-9.0777	229.9	-8.7102	215.5	-8.3473	197.9	-7.9887	178.8
2161	9.1196	142333.000	-8.641	248.4	-8.6307	246.8	-8.6002	244	-8.5518	240.1	-8.4101	229.4	-8.2206	215.1	-7.9947	198	-7.7411	178.7
2192	11.0518	145000.000	-9.0994	246.7	-8.9655	245.2	-8.8356	242.7	-8.708	239	-8.4556	228.7	-8.2012	214.8	-7.9404	198.1	-7.671	179
2223	11.0003	147666.000	-9.1014	245	-8.9764	243.5	-8.85	241	-8.7224	237.5	-8.4635	227.5	-8.1991	214	-7.9286	197.7	-7.6514	179
2251	10.1634	150333.000	-9.5986	243.8	-9.4127	242.2	-9.233	239.7	-9.0584	236.2	-8.7215	226.4	-8.396	213.1	-8.0775	197	-7.7625	178.8
2282	9.2155	153000.000	-9.5628	242.6	-9.4099	241	-9.2555	238.4	-9.1001	235	-8.787	225.3	-8.472	212.2	-8.1555	196.3	-7.8375	178.4
2312	9.5194	155666.000	-9.1692	241.4	-9.068	239.9	-8.8599	237.5	-8.6459	234	-8.6016	224.5	-8.3401	211.6	-8.0644	195.9	-7.7772	178.3
2343	8.9556	158333.000	-10.0834	240.2	-9.8549	238.7	-9.6378	236.3	-9.4303	232.9	-9.0378	222.5	-8.6671	208.9	-8.3108	195.3	-7.9633	178
2373	7.4129	161000.000	-10.1815	239.4	-9.9864	237.7	-9.7924	235.3	-9.5999	231.8	-9.2199	222.4	-8.8466	209.8	-8.4794	194.5	-8.1171	177.5
2404	6.4715	163666.000	-10.4801	238.7	-10.2661	237	-10.0559	234.4	-9.8491	231	-9.4444	221.6	-9.0497	209.1	-8.663	193.8	-8.2825	177
2435	6.5434	166333.000	-9.9727	237.9	-9.8442	236.3	-9.7074	233.8	-9.5636	230.4	-9.2592	221	-8.9378	208.6	-8.6042	193.4	-8.2617	176.7
2466	6.452	169000.000	-10.653	237.1	-10.4205	235.5	-10.197	233.1	-9.981	229.7	-9.5662	220.4	-9.1679	208	-8.7801	193.1	-8.399	176.4
2496	6.6039	171666.000	-9.8547	236.2	-9.7549	234.7	-9.6427	232.3	-9.52	229	-9.2492	219.8	-8.9528	207.6	-8.6375	192.8	-8.3081	176.3
2526	7.5059	174333.000	-9.9997	235.2	-9.8466	233.9	-9.694	231.6	-9.5411	228.4	-9.2325	218.4	-8.9182	207.3	-8.5968	192.8	-8.2678	176.3
2557	6.9046	177000.000	-10.5783	234.3	-10.3558	232.9	-10.1408	230.6	-9.9322	227.4	-9.5302	218.6	-8.7652	206.7	-8.393	192.3	-8.393	176.1
2588	6.9992	179666.000	-9.7779	233.4	-9.6398	232.1	-9.5386	229.8	-9.4261	226.7	-9.1737	218	-8.8931	206.3	-8.5914	192.1	-8.2737	176



# 1 Year Half Life

138 8	Time (Days)	Solute Mass Flux (mg/day)	Node 5 (meters)	Node 8 (meters)	Node 11 (meters)	Node 14 (meters)	Node 17 (meters)	Node 20 (meters)	Node 23 (meters)	Node 26 (meters)	3
0	0	0	1400	1400	1400	1400	1400	1400	1400	1400	0
5	0	0	14.5382	14.5382	14.5382	14.5382	14.5382	14.5382	14.5382	14.5382	0
10	0	0.0002	14.3945	14.3945	14.3945	14.3945	14.3945	14.3945	14.3945	14.3945	0
15	0	0.0003	14.285	14.285	14.285	14.285	14.285	14.285	14.285	14.285	0
20	0.0001	0.0001	14.194	14.194	14.194	14.194	14.194	14.194	14.194	14.194	0
25	0.0003	0.0015	14.115	14.115	14.115	14.115	14.115	14.115	14.115	14.115	0
31	0.0005	0.0043	14.0317	14.0317	14.0317	14.0317	14.0317	14.0317	14.0317	14.0317	0
60	-0.0008	-0.0198	-12.8871	-12.8871	-12.8871	-12.8871	-12.8871	-12.8871	-12.8871	-12.8871	0.1
91	0.001	0.0106	-11.8471	-11.8471	-11.8471	-11.8471	-11.8471	-11.8471	-11.8471	-11.8471	0.1
121	0.0022	0.0752	-11.5404	-11.5404	-11.5404	-11.5404	-11.5404	-11.5404	-11.5404	-11.5404	0.1
152	0.0027	1.7099	-11.3184	-11.3184	-11.3184	-11.3184	-11.3184	-11.3184	-11.3184	-11.3184	0
182	0.0035	7.8157	-11.3156	-11.3156	-11.3156	-11.3156	-11.3156	-11.3156	-11.3156	-11.3156	0.1
213	0.3332	18.1448	-12.2018	-12.2018	-12.2018	-12.2018	-12.2018	-12.2018	-12.2018	-12.2018	1.1
244	0.3269	28.2787	-12.5932	-12.5932	-12.5932	-12.5932	-12.5932	-12.5932	-12.5932	-12.5932	4.1
274	0.3242	38.0048	-12.29	-12.29	-12.29	-12.29	-12.29	-12.29	-12.29	-12.29	7.7
305	0.3737	49.5896	-12.2722	-12.2722	-12.2722	-12.2722	-12.2722	-12.2722	-12.2722	-12.2722	13.7
335	0.6335	68.594	-10.4255	-10.4255	-10.4255	-10.4255	-10.4255	-10.4255	-10.4255	-10.4255	16.6
366	1.051	101.1736	-10.9366	-10.9366	-10.9366	-10.9366	-10.9366	-10.9366	-10.9366	-10.9366	21
397	1.1366	138.4695	-11.477	-11.477	-11.477	-11.477	-11.477	-11.477	-11.477	-11.477	26.7
425	1.2274	170.8361	-10.6141	-10.6141	-10.6141	-10.6141	-10.6141	-10.6141	-10.6141	-10.6141	29.3
456	1.4676	216.3306	-10.6988	-10.6988	-10.6988	-10.6988	-10.6988	-10.6988	-10.6988	-10.6988	30.8
486	1.4211	258.9639	-11.3862	-11.3862	-11.3862	-11.3862	-11.3862	-11.3862	-11.3862	-11.3862	31.1
517	1.1899	295.2321	-11.677	-11.677	-11.677	-11.677	-11.677	-11.677	-11.677	-11.677	31
547	1.0891	327.9044	-11.2541	-11.2541	-11.2541	-11.2541	-11.2541	-11.2541	-11.2541	-11.2541	30.7
578	1.013	359.3073	-11.9015	-11.9015	-11.9015	-11.9015	-11.9015	-11.9015	-11.9015	-11.9015	30.1
609	0.8841	386.714	-11.7104	-11.7104	-11.7104	-11.7104	-11.7104	-11.7104	-11.7104	-11.7104	29.8
639	1.0157	417.1839	-10.8924	-10.8924	-10.8924	-10.8924	-10.8924	-10.8924	-10.8924	-10.8924	29.8
670	1.2661	458.4327	-10.6613	-10.6613	-10.6613	-10.6613	-10.6613	-10.6613	-10.6613	-10.6613	29.8
700	1.6349	505.4786	-9.5325	-9.5325	-9.5325	-9.5325	-9.5325	-9.5325	-9.5325	-9.5325	30.3
731	1.8748	563.5999	-10.0891	-10.0891	-10.0891	-10.0891	-10.0891	-10.0891	-10.0891	-10.0891	30.7
762	1.9699	624.6653	-9.284	-9.284	-9.284	-9.284	-9.284	-9.284	-9.284	-9.284	31
790	2.4635	693.6436	-8.0167	-8.0167	-8.0167	-8.0167	-8.0167	-8.0167	-8.0167	-8.0167	30.7
821	2.7937	780.2489	-8.5715	-8.5715	-8.5715	-8.5715	-8.5715	-8.5715	-8.5715	-8.5715	30.3
851	2.4377	853.3813	-8.3809	-8.3809	-8.3809	-8.3809	-8.3809	-8.3809	-8.3809	-8.3809	30.5
882	2.0831	917.9565	-9.0352	-9.0352	-9.0352	-9.0352	-9.0352	-9.0352	-9.0352	-9.0352	28.1
912	1.7488	970.4191	-10.0656	-10.0656	-10.0656	-10.0656	-10.0656	-10.0656	-10.0656	-10.0656	26.7
943	1.352	1012.332	-10.1605	-10.1605	-10.1605	-10.1605	-10.1605	-10.1605	-10.1605	-10.1605	25.3
974	1.0694	1045.484	-10.7352	-10.7352	-10.7352	-10.7352	-10.7352	-10.7352	-10.7352	-10.7352	24
1004	1.0031	1075.576	-9.9274	-9.9274	-9.9274	-9.9274	-9.9274	-9.9274	-9.9274	-9.9274	22
1035	1.0695	1108.732	-10.0794	-10.0794	-10.0794	-10.0794	-10.0794	-10.0794	-10.0794	-10.0794	21.2
1065	1.2568	1146.435	-8.7555	-8.7555	-8.7555	-8.7555	-8.7555	-8.7555	-8.7555	-8.7555	20.4
1096	1.4539	1191.507	-8.9984	-8.9984	-8.9984	-8.9984	-8.9984	-8.9984	-8.9984	-8.9984	19.6
1127	1.488	1237.636	-8.5867	-8.5867	-8.5867	-8.5867	-8.5867	-8.5867	-8.5867	-8.5867	23.9
1155	1.4557	1278.395	-8.8657	-8.8657	-8.8657	-8.8657	-8.8657	-8.8657	-8.8657	-8.8657	27.9



## 1 Year Half Life

1186	1.3568	1320.454	-8.7151	33.8	-8.6247	33.4	-8.531	32.8	-8.4343	31.9	-8.2323	29.4	-8.0198	26.2	-7.7971	22.5	-7.5642	18.6
1216	1.1416	1354.702	-9.72	31.7	-9.5022	31.3	-9.2972	30.7	-9.1029	29.8	-8.7401	27.6	-8.4028	24.6	-8.0826	21.2	-7.7731	17.7
1247	0.8976	1382.526	-9.6843	29.7	-9.5231	29.3	-9.3607	28.7	-9.1979	27.9	-8.7825	25.8	-8.5492	23.1	-8.2283	19.9	-7.9096	16.7
1277	0.7503	1405.034	-10.1212	27.9	-9.9172	27.5	-9.7187	26.9	-9.5249	26.2	-9.1493	24.2	-8.7864	21.7	-8.4328	18.8	-8.086	15.8
1308	0.6065	1423.837	-10.4139	26.1	-10.2039	25.8	-9.9978	25.3	-9.7852	24.6	-9.3997	22.7	-9.0153	20.4	-8.6401	17.7	-8.272	14.9
1339	0.4754	1438.574	-10.8587	24.6	-10.6176	24.2	-10.385	23.7	-10.1581	23.1	-9.7194	21.3	-9.2978	19.1	-8.897	16.6	-8.4924	14
1369	0.3627	1449.454	-11.1477	23.2	-10.9051	22.8	-10.6673	22.3	-10.434	21.7	-9.9796	20.1	-9.5399	18	-9.1128	15.6	-8.696	13.2
1400	0.2813	1458.174	-11.3858	21.8	-11.1418	21.5	-10.9016	21	-10.6651	20.4	-10.2024	18.9	-9.752	16.9	-9.3125	14.7	-8.8822	12.4
1430	0.2573	1465.894	-11.118	20.6	-10.9324	20.3	-10.7422	19.8	-10.5483	19.3	-10.1525	17.8	-9.7498	15.9	-9.3435	13.8	-8.9356	11.7
1461	0.3486	1476.699	-10.0045	19.3	-9.949	19	-9.8759	18.7	-9.7871	18.1	-9.5694	16.8	-9.3086	14.2	-8.7414	13.1	-8.6947	11.1
1492	0.4691	1491.242	-9.7482	18	-9.6599	17.8	-9.5661	17.5	-9.4665	17	-9.2489	15.8	-9.0068	13.5	-8.75	11.8	-8.5239	10.1
1521	0.445	1504.148	-10.623	16.9	-10.3977	16.7	-10.1845	16.4	-9.981	16	-9.5959	14.9	-9.2302	13.5	-8.752	11.1	-8.4119	9.5
1552	0.4021	1516.614	-9.8784	15.8	-9.7834	15.7	-9.6769	15.4	-9.5606	15	-9.3044	14	-9.024	12.7	-8.7252	11.1	-8.4119	9.5
1582	0.5174	1532.137	-8.4621	14.8	-8.969	14.7	-8.8514	14.4	-8.738	14.1	-8.4479	13.2	-8.3312	12	-8.1666	10.6	-7.9624	9.1
1613	0.5955	1550.599	-9.0107	13.8	-8.8947	13.7	-8.7838	13.5	-8.6761	13.2	-8.4642	12.4	-8.2497	11.3	-8.0262	10.1	-7.7897	8.7
1643	0.5279	1566.436	-9.3869	12.9	-9.233	12.8	-9.0831	12.6	-8.9364	12.3	-8.6504	11.6	-8.3701	10.6	-8.0913	9.5	-7.8107	8.2
1674	0.406	1579.021	-10.1715	12.1	-9.9416	12	-9.722	11.8	-9.5114	11.6	-9.1128	10.9	-8.7374	10	-8.3785	8.9	-8.0309	7.8
1705	0.2864	1587.901	-10.6207	11.4	-10.3814	11.3	-10.1488	11.1	-9.9224	10.8	-9.4867	10.2	-9.0705	9.4	-8.6701	8.4	-8.2823	7.3
1735	0.247	1595.31	-10.1358	10.7	-9.9839	10.6	-9.8441	10.4	-9.6878	10.2	-9.3606	9.6	-9.0199	8.8	-8.6708	7.9	-8.3164	6.9
1766	0.2245	1602.268	-10.765	10.1	-10.5307	10	-10.3048	9.8	-10.0856	9.6	-9.6635	9	-9.2571	8.3	-8.8615	7.4	-8.4732	6.5
1796	0.244	1609.588	-9.4007	9.5	-9.3675	9.4	-9.3133	9.2	-9.241	9	-9.0521	8.5	-8.8172	7.8	-8.5482	7	-8.2539	6.1
1827	0.292	1618.641	-9.5956	8.9	-9.4697	8.8	-9.3445	8.7	-9.2187	8.5	-8.9624	8	-8.6962	7.4	-8.4179	6.6	-8.1266	5.8
1858	0.318	1628.498	-8.8915	8.3	-8.842	8.2	-8.7817	8.1	-8.7116	8	-8.5429	7.5	-8.3485	7	-8.1257	6.3	-7.8802	5.5
1886	0.3397	1638.01	-8.9321	7.8	-8.8358	7.7	-8.7383	7.6	-8.639	7.5	-8.4329	7.1	-8.2147	6.6	-7.9827	6	-7.7361	5.3
1917	0.3657	1649.347	-8.047	7.3	-8.0382	7.2	-8.0171	7.2	-7.9848	7	-7.8895	6.7	-7.7585	6.2	-7.5964	5.6	-7.4071	5
1947	0.3807	1660.767	-8.3593	6.8	-8.2618	6.8	-8.1669	6.7	-8.0731	6.6	-7.8853	6.3	-7.6927	5.8	-7.4914	5.3	-7.2787	4.7
1978	0.3614	1671.972	-8.1557	6.4	-8.0824	6.3	-8.0053	6.3	-7.9244	6.2	-7.7525	5.9	-7.5674	5.5	-7.3696	5	-7.159	4.5
2008	0.3284	1681.823	-8.6159	6	-8.4767	5.9	-8.342	5.9	-8.2107	5.8	-7.9556	5.5	-7.7061	5.2	-7.4583	4.7	-7.2091	4.2
2039	0.2624	1689.957	-9.3344	5.6	-9.1328	5.6	-8.9397	5.5	-8.754	5.4	-8.4017	5.2	-8.069	4.8	-7.7504	4.4	-7.4414	4
2070	0.1748	1701.8	-10.0035	5	-9.7713	4.9	-9.549	4.9	-9.3352	4.8	-8.9286	4.6	-8.5441	4.3	-8.176	3.9	-7.8197	3.5
2100	0.1402	1706.145	-10.0096	4.7	-9.8229	4.6	-9.6359	4.6	-9.4492	4.5	-9.0777	4.3	-8.7102	4	-8.3473	3.7	-7.9887	3.3
2131	0.1596	1710.935	-8.641	4.4	-8.6307	4.3	-8.6002	4.3	-8.5518	4.2	-8.4101	4	-8.2206	3.8	-7.9947	3.5	-7.7411	3.1
2161	0.1826	1716.594	-9.0994	4.1	-8.9655	4.1	-8.8356	4	-8.708	4	-8.4556	3.8	-8.2012	3.6	-7.9404	3.3	-7.671	3
2192	0.1715	1721.911	-9.1014	3.8	-8.9764	3.8	-8.85	3.8	-8.7224	3.7	-8.4635	3.6	-8.1991	3.3	-7.9286	3.1	-7.6514	2.8
2223	0.1504	1726.121	-9.5986	3.6	-9.4127	3.6	-9.2555	3.6	-9.0584	3.5	-8.7215	3.4	-8.396	3.2	-8.0775	2.9	-7.7625	2.6
2251	0.1287	1730.11	-9.5628	3.4	-9.4099	3.4	-9.2555	3.4	-9.1001	3.3	-8.787	3.2	-8.472	3	-8.1555	2.7	-7.8375	2.5
2282	0.1257	1733.88	-9.1682	3.2	-9.066	3.2	-8.9599	3.2	-8.8458	3.1	-8.6016	3	-8.3401	2.8	-8.0644	2.6	-7.7772	2.4
2312	0.1116	1737.338	-10.0834	3	-9.8549	3	-9.6378	3	-9.4303	2.9	-9.0378	2.8	-8.6671	2.6	-8.3108	2.4	-7.9633	2.2
2343	0.0873	1739.957	-10.1815	2.8	-9.9864	2.8	-9.7924	2.8	-9.5999	2.7	-9.2199	2.6	-8.8466	2.5	-8.4794	2.3	-8.1171	2.1
2373	0.0719	1742.187	-10.4801	2.7	-10.2661	2.6	-10.0559	2.6	-9.8491	2.6	-9.4444	2.5	-9.0497	2.3	-8.663	2.2	-8.2825	2
2404	0.0686	1744.315	-9.8727	2.5	-9.8442	2.5	-9.7074	2.5	-9.5636	2.4	-9.2592	2.3	-8.9378	2.2	-8.6042	2	-8.2617	1.9
2435	0.064	1746.234	-10.853	2.4	-10.4205	2.3	-10.197	2.3	-9.981	2.3	-9.5682	2.2	-9.1679	2.1	-8.7801	1.9	-8.399	1.7
2465	0.0618	1748.15	-9.8547	2.2	-9.7549	2.2	-9.6427	2.2	-9.52	2.2	-9.2492	2.1	-8.9528	1.9	-8.6375	1.8	-8.3081	1.6
2496	0.0684	1750.142	-9.8987	2.1	-9.8466	2.1	-9.694	2.1	-9.5411	2	-9.2325	1.9	-8.9182	1.7	-8.5968	1.6	-8.2678	1.5
2526	0.0576	1751.929	-10.5783	2	-10.3558	2	-10.1408	1.9	-9.9322	1.9	-9.5302	1.8	-9.1429	1.7	-8.7652	1.6	-8.393	1.5
2557	0.0551	1753.638	-9.7278	1.8	-9.6398	1.8	-9.5386	1.8	-9.4261	1.8	-9.1737	1.7	-8.8931	1.6	-8.5914	1.5	-8.2737	1.4

## 1 Year Half Life

2616	0.0606	1755.336	-9.7539	1.7	-9.6232	1.7	-9.4913	1.7	-9.3573	1.7	-9.082	1.6	-8.7956	1.5	-8.4976	1.4	-8.1882	1.3
2647	0.0635	1757.304	-9.3474	1.6	-9.2565	1.6	-9.1585	1.6	-9.0541	1.6	-8.8277	1.5	-8.5804	1.5	-8.3147	1.4	-8.0326	1.2
2677	0.0658	1759.278	-9.278	1.5	-9.1892	1.5	-9.0577	1.5	-8.9435	1.5	-8.7059	1.4	-8.4555	1.4	-8.1921	1.3	-7.9157	1.2
2708	0.0652	1761.299	-9.1469	1.4	-9.0413	1.4	-8.9324	1.4	-8.8204	1.4	-8.5867	1.3	-8.3404	1.3	-8.0818	1.2	-7.811	1.1
2738	0.0617	1763.151	-9.3151	1.4	-9.1778	1.4	-9.0413	1.4	-8.9052	1.3	-8.6326	1.3	-8.3573	1.2	-8.0773	1.1	-7.7912	1.1
2769	0.0518	1764.757	-9.9174	1.3	-9.7139	1.3	-9.5177	1.3	-9.3278	1.2	-9.063	1.2	-8.6131	1.1	-8.2729	1.1	-7.9385	1
2800	0.0408	1766.024	-10.1457	1.2	-9.9478	1.2	-9.7526	1.2	-9.5601	1.1	-9.2879	1.1	-8.8135	1.1	-8.4513	1	-8.0943	0.9
2830	0.0348	1767.089	-10.1683	1.1	-9.9887	1.1	-9.8086	1.1	-9.6284	1.1	-9.2679	1.1	-8.9081	1	-8.5492	1	-8.1911	0.9
2861	0.0327	1768.081	-10.0639	1.1	-9.9056	1.1	-9.7448	1.1	-9.5817	1	-9.2499	1	-8.912	1	-8.5692	0.9	-8.2224	0.8
2891	0.0366	1769.179	-9.2165	1	-9.1578	1	-9.0859	1	-9.002	1	-8.8031	0.9	-8.5702	0.9	-8.3102	0.8	-8.0285	0.8
2922	0.0407	1770.442	-9.3	0.9	-9.1838	0.9	-9.067	0.9	-8.9487	0.9	-8.7059	0.9	-8.4523	0.8	-8.1866	0.8	-7.9082	0.7
2953	0.0415	1771.727	-8.9973	0.9	-9.0988	0.9	-8.9148	0.9	-8.7158	0.9	-8.5033	0.8	-8.2734	0.8	-8.0273	0.8	-7.7662	0.7
2982	0.0421	1772.947	-8.6866	0.8	-9.0748	0.8	-8.8778	0.8	-8.6772	0.8	-8.4566	0.8	-8.1399	0.8	-7.9004	0.7	-7.6472	0.7
3013	0.0415	1774.234	-8.7501	0.8	-9.0555	0.8	-8.8579	0.8	-8.6572	0.8	-8.4244	0.7	-8.0231	0.7	-7.7874	0.7	-7.5392	0.6
3043	0.0436	1775.541	-8.0649	0.7	-9.0358	0.7	-8.8358	0.7	-8.6358	0.7	-8.4177	0.7	-8.1529	0.6	-7.9122	0.6	-7.6639	0.5
3074	0.0392	1776.758	-9.3559	0.7	-9.1391	0.7	-8.9374	0.7	-8.7482	0.7	-8.5399	0.7	-8.2727	0.6	-7.9936	0.6	-7.7291	0.6
3104	0.0313	1777.696	-9.1561	0.7	-9.02	0.7	-8.8803	0.6	-8.738	0.6	-8.4487	0.6	-8.1556	0.6	-7.8605	0.6	-7.5639	0.5
3135	0.0267	1778.524	-8.6351	0.6	-9.4442	0.6	-9.2587	0.6	-9.0777	0.6	-8.7268	0.6	-8.387	0.6	-8.0549	0.5	-7.7277	0.5
3166	0.0213	1779.184	-10.08	0.6	-9.8643	0.6	-9.6544	0.6	-9.4497	0.6	-9.0539	0.5	-8.6733	0.5	-8.3045	0.5	-7.9445	0.5
3196	0.0178	1779.719	-10.0406	0.5	-9.8625	0.5	-9.6833	0.5	-9.5033	0.5	-9.1427	0.5	-8.7827	0.5	-8.4242	0.5	-8.0674	0.4
3227	0.0172	1780.251	-9.8347	0.5	-9.6901	0.5	-9.5414	0.5	-9.3892	0.5	-9.0759	0.5	-8.7531	0.5	-8.4231	0.4	-8.0874	0.4
3257	0.0191	1780.823	-9.1704	0.5	-9.0862	0.5	-9.0152	0.5	-8.9225	0.5	-8.7116	0.5	-8.4722	0.4	-8.2097	0.4	-7.9282	0.4
3288	0.0222	1781.511	-8.7144	0.5	-8.6558	0.5	-8.5896	0.4	-8.516	0.4	-8.3477	0.4	-8.1529	0.4	-7.9342	0.4	-7.6939	0.4
3319	0.0259	1782.313	-7.9173	0.4	-7.9115	0.4	-7.8947	0.4	-7.8675	0.4	-7.834	0.4	-7.6635	0.4	-7.5112	0.4	-7.33	0.3
3347	0.0288	1783.119	-7.7255	0.4	-7.6886	0.4	-7.648	0.4	-7.6031	0.4	-7.4991	0.4	-7.3746	0.4	-7.2285	0.4	-7.0607	0.3
3378	0.0286	1784.006	-7.7654	0.4	-7.6988	0.4	-7.6273	0.4	-7.5565	0.4	-7.4092	0.4	-7.2524	0.3	-7.084	0.3	-6.9025	0.3
3408	0.0283	1784.794	-8.0129	0.4	-7.9091	0.4	-7.8068	0.4	-7.7056	0.3	-7.5046	0.3	-7.303	0.3	-7.0981	0.3	-6.8877	0.3
3439	0.023	1785.506	-8.2508	0.3	-8.1293	0.3	-8.0092	0.3	-7.8494	0.3	-7.6385	0.3	-7.4199	0.3	-7.1944	0.3	-6.9621	0.3
3469	0.0208	1786.129	-8.1483	0.3	-8.0513	0.3	-7.9516	0.3	-7.8408	0.3	-7.6285	0.3	-7.4216	0.3	-7.1876	0.3	-6.9515	0.3
3500	0.018	1786.686	-8.8561	0.3	-8.6771	0.3	-8.5057	0.3	-8.3408	0.3	-8.0285	0.3	-7.7276	0.3	-7.439	0.3	-7.1567	0.2
3531	0.015	1787.15	-8.9012	0.3	-8.7549	0.3	-8.6081	0.3	-8.4613	0.3	-8.168	0.3	-7.8761	0.3	-7.5856	0.2	-7.2961	0.2
3561	0.0122	1787.515	-8.6916	0.3	-8.4636	0.3	-8.2459	0.3	-8.0371	0.3	-7.8418	0.2	-7.6899	0.2	-7.5155	0.2	-7.339	0.2
3592	0.0096	1787.813	-9.7858	0.2	-9.5962	0.2	-9.4074	0.2	-9.22	0.2	-8.9499	0.2	-8.4868	0.2	-8.1308	0.2	-7.781	0.2
3622	0.0079	1788.051	-10.216	0.2	-9.9933	0.2	-9.7764	0.2	-9.5647	0.2	-9.1547	0.2	-8.7597	0.2	-8.3766	0.2	-8.0031	0.2
3653	0.0075	1788.285	-9.6093	0.2	-9.4931	0.2	-9.3673	0.2	-9.2336	0.2	-8.9472	0.2	-8.6421	0.2	-8.324	0.2	-7.9968	0.2
3684	0.0082	1788.541	-9.4411	0.2	-9.3218	0.2	-9.1987	0.2	-9.0717	0.2	-8.8064	0.2	-8.5272	0.2	-8.2356	0.2	-7.933	0.2
3712	0.0088	1788.787	-9.1655	0.2	-9.0678	0.2	-8.9644	0.2	-8.8558	0.2	-8.6239	0.2	-8.3744	0.2	-8.1092	0.2	-7.8301	0.2
3743	0.0079	1789.031	-10.0041	0.2	-9.7882	0.2	-9.5827	0.2	-9.3857	0.2	-9.0114	0.2	-8.6559	0.2	-8.3119	0.2	-7.9744	0.2
3773	0.0082	1789.216	-10.2037	0.2	-10.0035	0.2	-9.8059	0.2	-9.6109	0.2	-9.2284	0.2	-8.8549	0.2	-8.4887	0.2	-8.128	0.1
3804	0.0074	1789.444	-8.1461	0.2	-8.2061	0.2	-8.2377	0.2	-8.2444	0.2	-8.1944	0.2	-8.0763	0.1	-7.9058	0.1	-7.6949	0.1
3834	0.0098	1789.741	-7.9795	0.2	-7.9484	0.2	-7.9139	0.2	-7.8748	0.2	-7.7792	0.1	-7.6574	0.1	-7.5078	0.1	-7.3307	0.1
3865	0.0092	1790.027	-9.0653	0.1	-8.8799	0.1	-8.7967	0.1	-8.5435	0.1	-8.2404	0.1	-7.958	0.1	-7.687	0.1	-7.4202	0.1
3896	0.0087	1790.234	-9.845	0.1	-9.6126	0.1	-9.3905	0.1	-9.1779	0.1	-8.7769	0.1	-8.4021	0.1	-8.0473	0.1	-7.7067	0.1
3926	0.0048	1790.378	-10.1316	0.1	-9.9145	0.1	-9.7016	0.1	-9.4927	0.1	-9.087	0.1	-8.6961	0.1	-8.318	0.1	-7.9505	0.1
3957	0.0045	1790.518	-9.4168	0.1	-9.3166	0.1	-9.2052	0.1	-9.0846	0.1	-8.8207	0.1	-8.5343	0.1	-8.2321	0.1	-7.9186	0.1
3987	0.0057	1790.688	-8.3372	0.1	-8.3324	0.1	-8.3118	0.1	-8.2767	0.1	-8.1671	0.1	-8.0128	0.1	-7.8214	0.1	-7.5996	0.1
4018	0.0063	1790.884	-8.7548	0.1	-8.6378	0.1	-8.5241	0.1	-8.4125	0.1	-8.191	0.1	-7.9662	0.1	-7.7338	0.1	-7.4909	0.1



# Amendments

138	8	ute Mass Flux (mg/day)	(grams)	0.25	Node 8 (meters)	ppm	Node 11 (meters)	ppm	0.5	Node 14 (meters)	ppm	1	Node 17 (meters)	ppm	1.5	Node 20 (meters)	ppm	2	Node 23 (meters)	ppm	2.5	Node 26 (meters)	ppm	3
0	0	0	0	1400	-14.5	1400	-14.25	0	-14	-13.9267	-17.3	0	-13.5	0	-13	-12.9654	-1.1	0	-12.5	0	-12	0	0	
5	0	0	0	1408	-14.4038	1272.6	-14.1614	118.7	-13.9267	-17.3	-13.4497	4.4	-12.9654	4.4	-12.9654	-1.1	0	-12.5	0	-12.5	0	-11.9837	0	
10	0	0	0	1385.9	-14.3397	1118.5	-14.0986	273.9	-13.868	-19.7	-13.4002	4.2	-12.925	-0.9	-12.444	-0.2	-11.9584	0	-12.444	0.2	-11.9584	0	0	
15	0	0	0	1339.7	-14.2904	1026.5	-14.0498	362.4	-13.8209	4.6	-13.3574	-2.4	-12.872	0.8	-12.4114	-0.2	-11.9308	0	-12.4114	-0.2	-11.9308	0	0	
20	0	0	0	1290.7	-14.2496	969.2	-14.0092	411.3	-13.7812	39.6	-13.3202	2.4	-12.8307	2.4	-12.3807	-0.5	-11.9036	0.1	-12.3807	-0.5	-11.9036	0.1	0	
25	0	0.0001	0	1244.7	-14.2142	929.5	-13.974	440	-13.7466	76.1	-13.2872	-15.2	-12.8223	3	-12.3523	-0.6	-11.8778	0.1	-12.8223	-0.6	-11.8778	0.1	0	
31	0	0.0001	0	1194.5	-14.1773	893.9	-13.9373	461	-13.7103	116.5	-13.2523	-18	-12.7892	2.5	-12.3213	-0.3	-11.8492	0	-12.7892	-0.3	-11.8492	0	0	
60	0	-0.0003	0	943.3	-13.6827	759	-13.4558	518.6	-13.2585	286.7	-12.8541	27.5	-12.438	-3.1	-12.0115	0.5	-11.5761	0	-12.438	0.5	-11.5761	0	0	
91	0.0001	0.0021	0	723.8	-13.247	635.7	-13.0262	505.6	-12.8432	362.8	-12.468	126.3	-12.0812	20.7	-11.6839	1.5	-11.2768	0.1	-12.0812	1.5	-11.2768	0.1	0	
121	0.0009	0.0302	0	593.9	-13.1689	539.9	-12.9431	459.2	-12.7494	363.5	-12.3579	180	-11.9605	61.2	-11.5573	13.2	-11.1483	1.3	-11.9605	13.2	-11.1483	1.3	0	
152	0.0038	0.1488	0	507.8	-13.1464	470.1	-12.9185	412.6	-12.7201	343.1	-12.3203	199.3	-11.9164	89.5	-11.5082	29.8	-11.0957	5.2	-11.9164	29.8	-11.0957	5.2	0	
182	0.0075	0.3741	0	447.4	-13.2275	418.6	-12.9959	374.4	-12.7891	319.9	-12.3745	202.7	-11.9578	104.8	-11.5388	42.7	-11.1173	10.7	-11.9578	42.7	-11.1173	10.7	0	
213	0.0077	0.6127	0	408	-13.2702	382.2	-13.473	343.6	-12.873	276.1	-12.9813	183.6	-12.4994	103.9	-12.0207	48.2	-11.5446	16.5	-12.4994	48.2	-11.5446	16.5	0	
244	0.0049	0.7658	0	382.1	-13.9597	356.4	-13.7115	319.4	-13.467	276.1	-12.9813	183.6	-12.4994	103.9	-12.0207	48.2	-11.5446	16.5	-12.9813	48.2	-11.5446	16.5	0	
274	0.0048	0.9092	0	354.9	-13.8553	332.1	-13.6153	299	-13.3887	259.5	-12.9331	175.1	-12.4747	101.4	-12.0142	48.7	-11.5519	17.7	-12.4747	48.7	-11.5519	17.7	0	
305	0.006	1.0942	0	325.3	-13.8751	306.7	-13.634	278.4	-13.4054	243.7	-12.9473	168.1	-12.488	100.1	-12.0272	50.2	-11.5651	19.3	-12.9473	50.2	-11.5651	19.3	0	
335	0.0131	1.4861	0	289.8	-13.0324	276.7	-12.8199	255.6	-12.6543	228.2	-12.3077	164.6	-11.9434	103.4	-11.5637	55.7	-11.1709	23.3	-12.3077	55.7	-11.1709	23.3	0	
366	0.021	2.1376	0	257.8	-13.3179	247.8	-13.084	231.6	-12.873	210.4	-12.4521	158.7	-12.0313	105.7	-11.6093	61.2	-11.1852	28.7	-12.4521	61.2	-11.1852	28.7	0	
397	0.0168	2.6591	0	237.4	-13.6244	228	-13.3621	213.4	-13.1519	194.6	-12.6943	149.2	-12.2397	102.1	-11.7872	61.3	-11.3359	31.2	-12.6943	61.3	-11.3359	31.2	0	
425	0.018	3.164	0	218.8	-13.2509	210.9	-13.0259	198.3	-12.8326	181.9	-12.4382	141.7	-12.0345	99.3	-11.623	61.7	-11.2048	33	-12.4382	61.7	-11.2048	33	0	
456	0.0225	3.8608	0	198.9	-13.3357	192.5	-13.1029	182.1	-12.8939	168.3	-12.4745	134	-12.0529	96.6	-11.6288	62.4	-11.2019	35.3	-12.8939	96.6	-11.6288	35.3	0	
486	0.018	4.3994	0	184.6	-13.7072	178.6	-13.4623	169.1	-13.2264	156.6	-12.7588	125.8	-12.2955	92.1	-11.8354	60.9	-11.3775	35.9	-13.4623	60.9	-11.3775	35.9	0	
517	0.0118	4.7667	0	172.7	-13.876	166.8	-13.6309	157.8	-13.3934	146.2	-12.9202	117.9	-12.449	87	-11.9795	58.1	-11.5113	35.3	-13.876	58.1	-11.5113	35.3	0	
547	0.012	5.1273	0	160.7	-13.6908	155.6	-13.4552	147.5	-13.2388	137	-12.8018	111.2	-12.36	82.8	-11.9141	56.2	-11.4649	34.7	-13.6908	56.2	-11.4649	34.7	0	
578	0.0108	5.4611	0	149.7	-14.0129	145.1	-13.7847	137.7	-13.5208	128.2	-13.0367	104.6	-12.5565	78.6	-12.0792	54	-11.604	34	-14.0129	78.6	-12.0792	54	0	
609	0.0084	5.7202	0	140	-13.9255	135.7	-13.6846	128.9	-13.4559	120.1	-12.9965	98.3	-12.5346	74.3	-12.0708	51.5	-11.6053	32.9	-13.9255	74.3	-12.0708	51.5	0	
639	0.0129	6.1063	0	129.5	-13.5362	125.9	-13.3079	120.2	-13.1076	112.5	-12.6992	93	-12.2815	71.1	-11.8558	50.2	-11.4231	32.5	-13.5362	71.1	-11.8558	50.2	0	
670	0.0178	6.6568	0	118.8	-13.4365	115.9	-13.2059	111.1	-13.0013	104.5	-12.5882	87.6	-12.17	68.2	-11.7467	49.2	-11.3186	32.5	-13.4365	49.2	-11.3186	32.5	0	
700	0.0241	7.38	0	108.8	-12.909	105.4	-12.6937	102.4	-12.5222	96.9	-12.1684	82.4	-11.8017	65.4	-11.4233	48.3	-11.0346	32.9	-12.909	65.4	-11.4233	48.3	0	
731	0.026	8.187	0	99.7	-13.2231	97.6	-12.9892	94.2	-12.7783	89.5	-12.3582	77.1	-11.9388	62.2	-11.519	47	-11.0979	33	-13.2231	62.2	-11.519	47	0	
762	0.0256	8.9819	0	91.7	-12.8739	89.9	-12.6544	86.9	-12.4738	82.8	-12.1048	71.9	-11.7255	58.9	-11.3401	45.3	-10.9463	32.7	-12.8739	58.9	-11.3401	45.3	0	
790	0.0353	9.9709	0	84.1	-12.2787	82.6	-12.0751	80.1	-11.9285	76.7	-11.6225	67.6	-11.3009	56.3	-10.9652	44.3	-10.6167	32.8	-12.2787	56.3	-10.9652	44.3	0	
821	0.0375	11.1344	0	76.8	-12.628	75.5	-12.4031	73.4	-12.2119	70.5	-11.8305	62.8	-11.4491	53.1	-11.0662	42.7	-10.681	32.5	-12.628	53.1	-11.0662	42.7	0	
851	0.0271	11.9472	0	71.4	-13.1153	70.1	-12.877	68.1	-12.8563	65.5	-12.2198	58.5	-11.7883	49.9	-11.3603	40.4	-10.9348	31.3	-13.1153	49.9	-11.3603	40.4	0	
882	0.0218	12.6236	0	66.3	-12.9854	65.1	-12.7581	63.4	-12.5603	60.9	-12.1606	54.6	-11.7562	46.8	-11.3475	38.3	-10.935	30	-12.9854	60.9	-11.3475	38.3	0	
912	0.0167	13.1243	0	61.9	-13.5247	60.9	-13.2781	59.2	-13.0385	57	-12.5857	51.2	-12.0997	44	-11.6388	36.2	-11.1815	28.6	-13.5247	44	-11.6388	36.2	0	
943	0.0106	13.4534	0	58.1	-13.5649	57.1	-13.324	55.5	-13.0957	53.4	-12.6388	48	-12.1816	41.3	-11.7241	34.1	-11.2663	27.1	-13.5649	53.4	-11.7241	34.1	0	
974	0.0075	13.6873	0	54.5	-13.8244	53.6	-13.5764	52.1	-13.3323	50.1	-12.8473	45	-12.3656	38.9	-11.8866	32.1	-11.4056	25.7	-13.8244	53.6	-11.8866	32.1	0	
1004	0.0084	13.9406	0	51.1	-13.3877	50.2	-13.1582	48.9	-12.9546	47.1	-12.8473	45	-12.3656	38.9	-11.8866	32.1	-11.4056	25.7	-13.3877	50.2	-11.8866	32.1	0	
1035	0.0107	14.2731	0	47.6	-13.4241	46.9	-13.1875	45.7	-12.9692	44.1	-12.5311	39.9	-12.0906	34.7	-11.6474	29	-11.2014	23.3	-14.2731	46.9	-11.6474	29	0	
1065	0.0145	14.7068	0	44.2	-12.7259	43.6	-12.5117	42.6	-12.342	41.2	-11.9894	37.5	-11.9894	32.8	-11.2397	27.7	-10.8462	22.4	-12.7259	43.6	-11.9894	37.5	0	
1096	0.0174	15.2453	0	40.9	-12.823	40.4	-12.5948	39.6	-12.3957	38.4	-11.9954	35.1	-11.592	31	-11.1845	26.4	-10.7727	21.6	-12.823	40.4	-11.592	31	0	
1127	0.0167	15.7621	0	38	-12.6039	37.5	-12.3818	36.8	-12.195	35.7	-11.8155	32.8	-11.4285	29.1	-11.0345	25	-10.6338	20.6	-12.6039	37.5	-11.8155	32.8	0	
1155	0.0157	16.2023	0	35.5	-12.7389	35.1	-12.5081	34.4	-12.303	33.5	-11.8919	30.9	-11.4791	27.6	-11.0641	23.7	-10.6463	19.8	-12.7389	35.1	-11.4791	27.6	0	
1186	0.014	16.6349	0	33.1	-12.653	32.7	-12.4256	32.1	-12.227	31.2	-11.8261	28.9	-11.4204	25.9	-11.0101	22.4	-10.5952	18.8	-12.653	32.7	-11.8261	25.9	0	
1216	0.0103	16.9443	0	31	-13.1479	30.7	-12.902	30.1	-12.6637	29.3	-12.1926	27.1	-11.2733	24.3	-11.2662	21.1	-10.8078	17.8	-13.1479	30.7	-12.902	27.1	0	

# Amendments

1247	0.0069	17.1597	29.1	-13.1034	28.8	-12.8652	28.2	-12.6424	27.5	-12.1949	25.4	-11.7454	22.9	-11.2941	19.9	-10.8412	16.8
1277	0.0057	17.3306	27.4	-13.2836	27.1	-13.0392	26.5	-12.8034	25.8	-12.3333	23.9	-11.8646	21.5	-11.3668	18.8	-10.9295	15.9
1308	0.004	17.4541	25.7	-13.3796	25.4	-13.1344	24.9	-12.8962	24.3	-12.4203	22.5	-11.945	20.3	-11.4701	17.7	-10.9954	15
1339	0.0025	17.5322	24.2	-13.5389	23.9	-13.2898	23.5	-13.0427	22.9	-12.5503	21.2	-12.0601	19.1	-11.5716	16.7	-11.0843	14.2
1369	0.0013	17.5726	22.9	-13.6191	22.6	-13.3696	22.2	-13.1211	21.6	-12.6252	20	-12.1306	18	-11.6371	15.7	-11.1444	13.4
1400	0.0008	17.5969	21.6	-13.672	21.3	-13.4223	20.9	-13.1733	20.3	-12.6759	18.9	-12.1794	17	-11.6837	14.8	-11.1885	12.6
1430	0.0013	17.6356	20.4	-13.4918	20.1	-13.2495	19.7	-13.0167	19.2	-12.5477	17.8	-12.075	16	-11.5991	14	-11.1206	11.9
1461	0.0039	17.7563	19.1	-12.9171	18.9	-12.6917	18.5	-12.4964	18	-12.0955	16.8	-11.6825	15.1	-11.2589	13.3	-10.8263	11.3
1492	0.0061	17.945	17.8	-12.7722	17.6	-12.5431	17.3	-12.3407	16.9	-11.9311	15.8	-11.5152	14.3	-11.0932	12.6	-10.6653	10.8
1521	0.0047	18.0809	16.7	-13.1902	16.6	-12.9429	16.3	-12.7013	15.9	-12.223	14.9	-11.7494	13.5	-11.2792	11.9	-10.8111	10.2
1552	0.004	18.2054	15.7	-12.822	15.5	-12.5919	15.3	-12.3866	14.9	-11.9699	14	-11.5434	12.7	-11.1112	11.2	-10.6732	9.7
1582	0.0068	18.4109	14.6	-12.1221	14.5	-11.911	14.3	-11.7463	14	-11.4037	13.1	-11.0453	12	-10.6728	10.7	-10.2878	9.2
1613	0.0076	18.6457	13.6	-12.4013	13.5	-12.1697	13.3	-11.9625	13.1	-11.5486	12.3	-11.1342	11.3	-10.7182	10.1	-10.2995	8.8
1643	0.0055	18.8109	12.8	-12.5991	12.7	-12.362	12.5	-12.1424	12.2	-11.7038	11.5	-11.2657	10.6	-10.8273	9.5	-10.3882	8.3
1674	0.0034	18.9171	12	-12.9813	11.9	-12.7336	11.7	-12.4907	11.5	-12.0093	10.8	-11.5326	10	-11.0594	8.9	-10.5889	7.8
1705	0.0017	18.9713	11.3	-13.1731	11.2	-12.942	11	-12.6775	10.8	-12.1867	10.2	-11.6986	9.4	-11.2129	8.4	-10.7291	7.3
1735	0.0018	19.0247	10.7	-12.9002	10.6	-12.6538	10.4	-12.4442	10.2	-11.9998	9.6	-11.5495	8.8	-11.0944	7.9	-10.6352	6.9
1766	0.0017	19.0772	10	-13.1597	9.9	-12.9112	9.8	-12.6658	9.6	-12.1778	9	-11.6925	8.3	-11.2091	7.5	-10.7269	6.6
1796	0.0024	19.1498	9.4	-12.4631	9.3	-12.2411	9.2	-12.0523	9	-11.6626	8.5	-11.2589	7.9	-10.8435	7.1	-10.4181	6.2
1827	0.0034	19.2563	8.8	-12.5318	8.7	-12.2978	8.6	-12.0847	8.5	-11.6568	8	-11.2261	7.4	-10.7921	6.7	-10.3545	5.9
1858	0.0037	19.3708	8.2	-12.179	8.2	-11.9559	8.1	-11.7654	7.9	-11.3768	7.5	-10.9792	7	-10.5733	6.3	-10.16	5.6
1886	0.004	19.4826	7.8	-12.2015	7.7	-11.9723	7.6	-11.7695	7.5	-11.3612	7.1	-10.9492	6.6	-10.532	6	-10.113	5.3
1917	0.0044	19.6184	7.2	-11.7763	7.2	-11.5604	7.1	-11.3848	7	-11.0248	6.6	-10.6539	6.2	-10.2731	5.6	-9.8833	5
1947	0.0045	19.7571	6.8	-11.9482	6.7	-11.7199	6.6	-11.5192	6.5	-11.1167	6.2	-10.7122	5.8	-10.3049	5.3	-9.8844	4.7
1978	0.0039	19.8738	6.3	-11.8628	6.3	-11.6381	6.2	-11.4443	6.1	-11.0525	5.8	-10.6555	5.5	-10.2535	5	-9.8465	4.5
2008	0.0034	19.9744	5.9	-12.1013	5.9	-11.8629	5.8	-11.6527	5.7	-11.2251	5.5	-10.7976	5.1	-10.3696	4.7	-9.8403	4.2
2039	0.0022	20.0442	5.6	-12.45	5.5	-12.2064	5.5	-11.9722	5.4	-11.507	5.1	-11.0453	4.8	-10.5859	4.4	-10.1282	4
2070	0.0017	20.0965	5.2	-12.3874	5.2	-12.1506	5.1	-11.9303	5.1	-11.4873	4.8	-11.0416	4.5	-10.5935	4.2	-10.1431	3.7
2100	0.0013	20.1343	4.9	-12.708	4.9	-12.4598	4.8	-12.2154	4.8	-11.7303	4.6	-11.2489	4.3	-10.7703	3.9	-10.2936	3.5
2131	0.0009	20.1612	4.6	-12.6581	4.6	-12.4159	4.6	-12.1836	4.5	-11.7175	4.3	-11.2497	4	-10.7804	3.7	-10.3099	3.3
2161	0.0016	20.2096	4.4	-11.9504	4.3	-11.7323	4.3	-11.5513	4.2	-11.1769	4	-10.7878	3.8	-10.3862	3.5	-9.9738	3.2
2192	0.002	20.2732	4.1	-12.1453	4.1	-11.9107	4	-11.696	4	-11.2664	3.8	-10.8357	3.6	-10.4029	3.3	-9.9676	3
2223	0.0017	20.326	3.8	-12.1286	3.8	-11.8952	3.8	-11.6825	3.7	-11.2546	3.6	-10.8236	3.4	-10.3952	3.1	-9.9522	2.8
2251	0.0014	20.3641	3.6	-12.352	3.6	-12.1102	3.6	-11.8796	3.5	-11.42	3.4	-10.9619	3.2	-10.5044	2.9	-10.0471	2.7
2282	0.0011	20.3978	3.4	-12.3084	3.4	-12.0709	3.3	-11.8489	3.3	-11.4029	3.2	-10.9543	3	-10.5033	2.8	-10.0437	2.5
2312	0.0012	20.4344	3.2	-12.093	3.2	-11.8625	3.2	-11.6555	3.1	-11.2363	3	-10.8109	2.8	-10.3799	2.6	-9.9437	2.4
2343	0.001	20.4649	3	-12.5078	3	-12.2601	3	-12.017	2.9	-11.5352	2.8	-11.0577	2.6	-10.5833	2.5	-10.111	2.2
2373	0.0006	20.4829	2.8	-12.522	2.8	-12.2787	2.8	-12.044	2.8	-11.574	2.6	-11.1033	2.5	-10.6321	2.3	-10.1604	2.1
2404	0.0005	20.4978	2.7	-12.6241	2.7	-12.3782	2.6	-12.138	2.6	-11.6584	2.5	-11.1793	2.4	-10.7005	2.2	-10.2219	2
2435	0.0006	20.5155	2.5	-12.3474	2.5	-12.1125	2.5	-11.8957	2.4	-11.4566	2.3	-11.0115	2.2	-10.5612	2.1	-10.1062	1.9
2465	0.0005	20.5315	2.4	-12.637	2.4	-12.3886	2.3	-12.1437	2.3	-11.8569	2.2	-11.1732	2.1	-10.6916	1.9	-10.2113	1.8
2496	0.0006	20.549	2.2	-12.2329	2.2	-12.0017	2.2	-11.7925	2.2	-11.3669	2.1	-10.9332	2	-10.4925	1.8	-10.0459	1.7
2526	0.0007	20.5704	2.1	-12.2822	2.1	-12.0441	2.1	-11.8213	2	-11.3745	2	-10.9256	1.9	-10.4743	1.7	-10.0206	1.6
2557	0.0005	20.586	2	-12.5356	2	-12.2887	1.9	-12.0466	1.9	-11.5651	1.8	-11.086	1.8	-10.6086	1.6	-10.1324	1.5
2588	0.0005	20.6027	1.9	-12.1197	1.8	-11.89	1.8	-11.6841	1.8	-11.265	1.7	-10.8372	1.6	-10.4021	1.5	-9.9608	1.4
2616	0.0007	20.6222	1.8	-12.125	1.7	-11.89	1.7	-11.6737	1.7	-11.239	1.6	-10.801	1.6	-10.3598	1.5	-9.9153	1.3
2647	0.0007	20.645	1.6	-11.9384	1.6	-11.7089	1.6	-11.504	1.6	-11.0893	1.5	-10.6687	1.5	-10.2425	1.4	-9.8111	1.3
2677	0.0008	20.6681	1.6	-11.9183	1.5	-11.6867	1.5	-11.4776	1.5	-11.0565	1.5	-10.6318	1.4	-10.2032	1.3	-9.7708	1.2
2708	0.0007	20.691	1.5	-11.8717	1.4	-11.6407	1.4	-11.4328	1.4	-11.0138	1.4	-10.5908	1.3	-10.1639	1.2	-9.7332	1.1

## Amendments

2738	0.0007	20.711	1.4	-11.9654	1.4	-11.7301	1.4	-11.5133	1.3	-11.0787	1.3	-10.6425	1.2	-10.2045	1.2	-9.7643	1.1
2769	0.0005	20.7259	1.3	-12.2525	1.3	-12.0082	1.3	-11.7722	1.3	-11.3028	1.2	-10.8358	1.2	-10.3704	1.1	-9.9061	1
2800	0.0003	20.7357	1.2	-12.3432	1.2	-12.0995	1.2	-11.8642	1.2	-11.3939	1.1	-10.9238	1.1	-10.4538	1	-9.9837	0.9
2830	0.0003	20.7438	1.1	-12.3271	1.1	-12.0857	1.1	-11.855	1.1	-11.3923	1.1	-10.9279	1	-10.4619	1	-9.9945	0.9
2861	0.0003	20.7526	1.1	-12.249	1.1	-12.0103	1.1	-11.7853	1	-11.333	1	-10.8776	1	-10.4193	0.9	-9.9585	0.8
2891	0.0004	20.7647	1	-11.8331	1	-11.6077	1	-11.4108	1	-11.009	1	-10.5974	0.9	-10.1774	0.9	-9.7498	0.8
2922	0.0005	20.7796	1	-11.8717	0.9	-11.5389	0.9	-11.4275	0.9	-11.0026	0.9	-10.5745	0.9	-10.1431	0.8	-9.708	0.7
2953	0.0005	20.7942	0.9	-11.7371	0.9	-11.5033	0.9	-11.305	0.9	-10.8938	0.8	-10.4773	0.8	-10.0557	0.8	-9.6291	0.7
2982	0.0005	20.8082	0.8	-11.6898	0.8	-11.4606	0.8	-11.2564	0.8	-10.8447	0.8	-10.4285	0.8	-10.0079	0.7	-9.5831	0.7
3013	0.0005	20.8227	0.8	-11.6528	0.8	-11.4237	0.8	-11.2197	0.8	-10.8085	0.7	-10.3932	0.7	-9.9736	0.7	-9.55	0.6
3043	0.0005	20.8382	0.7	-11.3465	0.7	-11.1272	0.7	-10.9433	0.7	-10.568	0.7	-10.1838	0.7	-9.7915	0.6	-9.3916	0.6
3074	0.0004	20.8509	0.7	-11.9936	0.7	-11.7477	0.7	-11.5095	0.7	-11.0394	0.7	-10.5758	0.6	-10.1168	0.6	-9.6608	0.6
3104	0.0003	20.859	0.7	-11.9003	0.7	-11.6653	0.7	-11.4484	0.6	-11.0116	0.6	-10.5716	0.6	-10.1287	0.6	-9.6834	0.5
3135	0.0002	20.8662	0.6	-12.1146	0.6	-11.872	0.6	-11.6394	0.6	-11.1756	0.6	-10.7129	0.6	-10.2508	0.5	-9.7889	0.5
3166	0.0002	20.8709	0.6	-12.295	0.6	-12.049	0.6	-11.8088	0.6	-11.3299	0.6	-10.8527	0.5	-10.3767	0.5	-9.9015	0.5
3196	0.0001	20.8746	0.5	-12.2371	0.5	-11.9959	0.5	-11.7654	0.5	-11.3025	0.5	-10.8376	0.5	-10.3707	0.5	-9.9022	0.4
3227	0.0001	20.8791	0.5	-12.1031	0.5	-11.8662	0.5	-11.6449	0.5	-11.1991	0.5	-10.7491	0.5	-10.2955	0.4	-9.8385	0.4
3257	0.0002	20.8853	0.5	-11.7683	0.5	-11.5412	0.5	-11.3407	0.5	-10.9327	0.5	-10.5163	0.4	-10.0924	0.4	-9.6618	0.4
3288	0.0003	20.8936	0.5	-11.5522	0.5	-11.3275	0.5	-11.1327	0.4	-10.7371	0.4	-10.3341	0.4	-9.9243	0.4	-9.5078	0.4
3319	0.0003	20.9038	0.4	-11.1926	0.4	-10.9765	0.4	-10.7991	0.4	-10.4363	0.4	-10.0633	0.4	-9.6809	0.4	-9.2899	0.3
3347	0.0004	20.9139	0.4	-11.1356	0.4	-10.9162	0.4	-10.7323	0.4	-10.3599	0.4	-9.9812	0.4	-9.5964	0.4	-9.2053	0.3
3378	0.0003	20.9243	0.4	-11.2058	0.4	-10.9821	0.4	-10.7894	0.4	-10.4014	0.4	-10.0096	0.3	-9.6138	0.3	-9.2137	0.3
3408	0.0003	20.9328	0.4	-11.3695	0.4	-11.1405	0.4	-10.9369	0.3	-10.5288	0.3	-10.119	0.3	-9.7072	0.3	-9.2928	0.3
3439	0.0002	20.94	0.3	-11.5132	0.3	-11.2814	0.3	-11.0717	0.3	-10.6515	0.3	-10.2299	0.3	-9.8067	0.3	-9.3814	0.3
3469	0.0002	20.9462	0.3	-11.4743	0.3	-11.2459	0.3	-11.043	0.3	-10.634	0.3	-10.221	0.3	-9.804	0.3	-9.3833	0.3
3500	0.0002	20.9514	0.3	-11.8178	0.3	-11.5773	0.3	-11.3497	0.3	-10.8969	0.3	-10.4463	0.3	-9.9971	0.3	-9.5485	0.2
3531	0.0001	20.9553	0.3	-11.8208	0.3	-11.5846	0.3	-11.3653	0.3	-10.9249	0.3	-10.4824	0.3	-10.0378	0.2	-9.5913	0.2
3561	0.0001	20.958	0.3	-12.1667	0.3	-11.919	0.3	-11.6759	0.3	-11.1932	0.3	-10.7144	0.2	-10.2385	0.2	-9.7646	0.2
3592	0.0001	20.9598	0.2	-12.1611	0.2	-11.9185	0.2	-11.685	0.2	-11.2172	0.2	-10.7484	0.2	-10.2786	0.2	-9.8079	0.2
3622	0	20.9613	0.2	-12.3077	0.2	-12.0606	0.2	-11.8179	0.2	-11.3336	0.2	-10.8507	0.2	-10.3687	0.2	-9.8873	0.2
3653	0.0001	20.963	0.2	-11.9695	0.2	-11.7362	0.2	-11.5223	0.2	-11.0882	0.2	-10.6472	0.2	-10.2001	0.2	-9.7479	0.2
3684	0.0001	20.9656	0.2	-11.8555	0.2	-11.622	0.2	-11.4083	0.2	-10.9772	0.2	-10.5413	0.2	-10.1009	0.2	-9.6562	0.2
3712	0.0001	20.9683	0.2	-11.7101	0.2	-11.4797	0.2	-11.2725	0.2	-10.8537	0.2	-10.4292	0.2	-9.9994	0.2	-9.5647	0.2
3743	0.0001	20.9706	0.2	-12.0929	0.2	-11.8467	0.2	-11.6071	0.2	-11.1312	0.2	-10.6589	0.2	-10.1891	0.2	-9.7208	0.2
3773	0	20.9719	0.2	-12.1633	0.2	-11.9192	0.2	-11.6828	0.2	-11.2102	0.2	-10.7377	0.2	-10.2652	0.2	-9.7927	0.1
3804	0.0001	20.9746	0.2	-11.1912	0.2	-10.9821	0.2	-10.8183	0.2	-10.4751	0.2	-10.1134	0.2	-9.7359	0.1	-9.3448	0.1
3834	0.0001	20.9787	0.2	-11.1351	0.2	-10.9156	0.2	-10.7315	0.2	-10.3586	0.1	-9.9791	0.1	-9.5927	0.1	-9.1993	0.1
3865	0.0001	20.9819	0.1	-11.6968	0.1	-11.4554	0.1	-11.2263	0.1	-10.773	0.1	-10.3243	0.1	-9.8788	0.1	-9.435	0.1
3896	0.0001	20.9836	0.1	-12.0778	0.1	-11.8298	0.1	-11.5859	0.1	-11.1023	0.1	-10.6234	0.1	-10.1482	0.1	-9.6759	0.1
3926	0	20.9845	0.1	-12.1923	0.1	-11.9462	0.1	-11.7054	0.1	-11.2248	0.1	-10.7455	0.1	-10.2672	0.1	-9.7898	0.1
3957	0	20.9857	0.1	-11.8293	0.1	-11.5982	0.1	-11.389	0.1	-10.964	0.1	-10.5313	0.1	-10.0921	0.1	-9.6473	0.1
3987	0.0001	20.9878	0.1	-11.3102	0.1	-11.093	0.1	-10.9127	0.1	-10.5421	0.1	-10.1592	0.1	-9.7653	0.1	-9.3616	0.1
4018	0.0001	20.9901	0.1	-11.525	0.1	-11.2928	0.1	-11.0826	0.1	-10.6619	0.1	-10.24	0.1	-9.816	0.1	-9.3895	0.1

138 8	Solute Mass Flux (mg/day)	Node 5 (meters)	Node 8 (meters)	Node 11 (meters)	Node 14 (meters)	Node 17 (meters)	Node 20 (meters)	Node 23 (meters)	Node 26 (meters)	Node 29 (meters)
Time (Days)	0	14.75	14.00	14.00	14.00	14.00	14.00	14.00	14.00	14.00
3	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0
60	0	0	0	0	0	0	0	0	0	0
91	0	0	0	0	0	0	0	0	0	0
121	-0.0001	-0.0029	-16.7614	685.8	-18.4712	685.8	-18.4712	685.8	-18.4712	685.8
152	-0.007	-0.22	-18.3651	440.4	-18.0496	329.8	-19.1619	329.8	-19.1619	329.8
182	-0.0392	-1.3954	-19.4867	248	-20.2242	248	-20.2242	248	-20.2242	248
213	-0.0872	-4.0904	-20.5644	200.6	-20.8802	200.6	-20.8802	200.6	-20.8802	200.6
244	-0.1223	-7.8904	-20.8802	168	-20.3331	168	-20.3331	168	-20.3331	168
274	-0.1315	-11.8344	-20.8471	147.2	-19.1583	147.2	-19.1583	147.2	-19.1583	147.2
305	-0.0833	-17.935	-17.8709	135.7	-17.6256	135.7	-17.6256	135.7	-17.6256	135.7
335	-0.0557	-19.6611	-17.21	123.8	-16.9532	123.8	-16.9532	123.8	-16.9532	123.8
366	-0.0322	-21.8961	-16.1866	106.6	-15.9411	106.6	-15.9411	106.6	-15.9411	106.6
397	-0.043	-20.9845	-16.8504	89.1	-17.2535	89.1	-17.2535	89.1	-17.2535	89.1
425	-0.0206	-22.5336	-15.7429	76.4	-18.7253	76.4	-18.7253	76.4	-18.7253	76.4
456	-0.0336	-23.5417	-17.5593	66.8	-19.5969	66.8	-19.5969	66.8	-19.5969	66.8
486	-0.082	-25.4638	-19.0513	58.1	-20.4495	58.1	-20.4495	58.1	-20.4495	58.1
517	-0.0827	-30.3367	-20.7874	51.3	-20.8462	51.3	-20.8462	51.3	-20.8462	51.3
547	-0.0817	-32.8704	-20.9723	46.2	-20.2419	46.2	-20.2419	46.2	-20.2419	46.2
578	-0.0735	-35.0754	-20.5464	41.9	-18.8258	41.9	-18.8258	41.9	-18.8258	41.9
609	-0.0576	-36.8623	-19.0961	38.7	-17.4985	38.7	-17.4985	38.7	-17.4985	38.7
639	-0.0389	-38.0287	-17.7452	35.9	-16.8733	35.9	-16.8733	35.9	-16.8733	35.9
670	-0.0174	-39.3735	-16.2763	33.4	-16.0353	33.4	-16.0353	33.4	-16.0353	33.4
700	-0.0072	-39.8211	-16.0835	29	-15.8294	29	-15.8294	29	-15.8294	29
731	-0.0192	-40.3982	-17.9383	26.7	-17.8262	26.7	-17.8262	26.7	-17.8262	26.7
762	-0.0294	-41.3101	-18.913	23.9	-18.6013	23.9	-18.6013	23.9	-18.6013	23.9
790	-0.0345	-42.3461	-20.2257	21.6	-19.8876	21.6	-19.8876	21.6	-19.8876	21.6
821	-0.0363	-43.4717	-20.7353	19.5	-20.4058	19.5	-20.4058	19.5	-20.4058	19.5
851	-0.035	-44.5567	-21.1665	17.6	-20.8341	17.6	-20.8341	17.6	-20.8341	17.6
882	-0.0314	-45.4986	-20.629	16.1	-20.3262	16.1	-20.3262	16.1	-20.3262	16.1
912	-0.0247	-46.2651	-19.417	14.9	-19.1398	14.9	-19.1398	14.9	-19.1398	14.9
943	-0.0169	-46.7717	-17.941	13.8	-17.6962	13.8	-17.6962	13.8	-17.6962	13.8
974	-0.0107	-47.105	-17.1873	12.8	-16.9368	12.8	-16.9368	12.8	-16.9368	12.8
1004	-0.0068	-47.3164	-16.4143	12	-16.1731	12	-16.1731	12	-16.1731	12
1035	-0.0042	-47.4333	-16.0363	11.3	-15.7908	11.3	-15.7908	11.3	-15.7908	11.3
1065	-0.0088	-47.8361	-18.4194	10.5	-16.3001	10.5	-16.3001	10.5	-16.3001	10.5
1096	-0.0129	-48.2362	-19.5027	8.9	-19.1833	8.9	-19.1833	8.9	-19.1833	8.9
1127	-0.0143	-48.6658	-20.3739	8.1	-20.0466	8.1	-20.0466	8.1	-20.0466	8.1
1155	-0.0145	-49.1154	-21.0039	7.4	-20.6754	7.4	-20.6754	7.4	-20.6754	7.4
1186	-0.0143	-49.1154	-21.0039	7.4	-20.6754	7.4	-20.6754	7.4	-20.6754	7.4
1216	-0.0143	-49.1154	-21.0039	7.4	-20.6754	7.4	-20.6754	7.4	-20.6754	7.4
1247	-0.0143	-49.1154	-21.0039	7.4	-20.6754	7.4	-20.6754	7.4	-20.6754	7.4
1277	-0.0143	-49.1154	-21.0039	7.4	-20.6754	7.4	-20.6754	7.4	-20.6754	7.4
1308	-0.0143	-49.1154	-21.0039	7.4	-20.6754	7.4	-20.6754	7.4	-20.6754	7.4

**APPENDIX C.**  
**CLIMATOLOGICAL DATA**

STATION NUMBER 353847 ELEMENT: DAILY MEAN TEMPERATURE  
 QUANTITY: MONTHLY AVERAGE

STATION: Hermiston, Oregon

FROM DATA WITH UNITS: DEGREES F

a = 1 day missing, b = 2 days missing, c = 3 days, ..etc., z = 26 or more days missing, A = Accumulations present  
 Long-term means based on columns; thus, the monthly row may not sum (or average) to the long-term annual value.

MAXIMUM ALLOWABLE NUMBER OF MISSING DAYS : 9

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	ANN
1984	33.53	40.00	47.47	50.02	55.32	63.42	71.84	71.00	60.22	49.23	41.70	29.71	51.12
1985	28.05	31.79	44.15	54.23	60.81	66.18	76.56	68.52	57.75	50.92	29.42	22.10	49.21
1986	34.31	39.50	49.35	50.78	59.68	71.00	68.66	75.11	60.42	53.02	43.40	32.98	53.18
1987	31.56	39.98	47.90	55.23	62.23	67.62	71.27	69.74	65.68	51.90	43.37	34.95	53.45
1988	33.34	40.79	46.06	53.72	59.52	65.45	73.66	70.73	63.52	57.89	46.27	34.19	53.76
1989	39.16	26.09	44.03	54.62	59.66	9999.00z	72.05	70.94	63.55	52.40	45.52	34.39	51.13a
1990	40.61	38.38	45.71	55.62	58.82	66.88	75.11	71.98	66.88	50.44	45.33	25.13	53.41
1991	9999.00z	44.16	9999.00z	9999.00z	9999.00z	9999.00z	9999.00z	9999.00z	9999.00z	9999.00z	9999.00z	9999.00z	44.16k
1992	9999.00z	9999.00z	9999.00z	56.27	64.08	73.03	73.61	74.74	62.75	54.13	42.77	33.61	59.44c
1993	23.98	30.91	42.16	53.03	65.31	66.47	69.03	70.69	64.63	54.92	35.12	36.90	51.10
1994	40.16	36.34	45.97	56.97	63.40a	66.77	77.42	75.18	68.17	52.47	40.42	9999.00z	56.66a
MEAN	33.86	36.79	45.87	54.05	60.88	67.42	72.92	71.86	63.36	52.73	41.33	31.55	52.18
S.D.	5.60	5.53	2.21	2.25	2.94	2.90	2.93	2.35	3.21	2.47	5.27	4.94	1.72
SKREW	-0.35	-0.70	-0.09	-0.61	-0.22	0.79	0.04	0.38	-0.22	0.69	-1.32	-0.96	-0.70
MAX	40.61	44.16	49.35	56.97	65.31	73.03	77.42	75.18	68.17	57.89	46.27	36.90	53.76
MIN	23.98	26.09	42.16	50.02	55.32	63.42	68.66	68.52	57.75	49.23	29.42	22.10	49.21
YRS	9	10	9	10	10	9	10	10	10	10	10	9	7



MONTHLY SUM

QUANTITY:

STATION NUMBER 353847 ELEMENT: DAILY PRECIPITATION FROM DATA WITH UNITS: INCHES

a=1 day missing, b=2 days missing, c=3 days, etc.,

z=26 or more days missing, A=Accumulations present

Long-term means based on columns; thus, the monthly row may not sum (or average) to the long-term annual value.

MAXIMUM ALLOWABLE NUMBER OF MISSING DAYS: 5

YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	ANN
1984	0.43	1.09	1.41	1.10	1.02	0.77	0.00	0.02	0.42	0.36	2.02	0.63	9.27
1985	0.25b	1.13	0.74	0.12	0.14	0.64	0.00	0.39	1.04	0.89	1.79	0.63	7.76
1986	1.57	2.38	1.11	0.37	1.09	0.01	0.37	0.02	1.00	0.56	1.92	0.99	11.39
1987	1.45	0.76	1.09	0.05	0.51	0.19	0.18	0.00	0.00	0.00	0.35	1.31	5.89
1988	0.97	0.01	0.98	2.16	0.76	0.50	0.01	0.00	0.65	0.00	1.51	0.69	8.24
1989	1.38	0.96	1.84	0.98	1.27	0.00z	0.19	0.59	0.00	0.34	1.78	0.64	9.97a
1990	0.76a	0.29	0.55	0.96	0.00f	0.28	0.15	0.74	0.00	0.96	0.50	0.07d	5.26a
1991	0.00z	0.67	0.00z	0.00z	0.00z	0.00z	0.00z	0.00z	0.00z	0.00z	0.00z	0.00z	0.67k
1992	0.00z	0.00z	0.00z	1.66	0.03	0.71	0.27	0.13	0.39	0.61	1.19a	1.31	6.30c
1993	1.88b	1.61	1.32	0.98	0.83	1.06	0.34	0.63	0.02	0.32	0.09	0.80	9.88
1994	0.79a	0.97	0.08	0.24	2.48	1.60	0.25	0.00	0.14	0.98a	1.83	0.00z	9.36a
MEAN	1.05	0.99	1.01	0.86	0.90	0.64	0.18	0.25	0.37	0.50	1.30	0.79	8.74
S.D.	0.55	0.66	0.51	0.69	0.72	0.48	0.14	0.30	0.41	0.36	0.72	0.38	1.89
SKEW	0.00	0.66	-0.27	0.51	0.98	0.67	-0.12	0.57	0.65	0.00	-0.65	-0.19	-0.13
MAX	1.88	2.38	1.84	2.16	2.48	1.60	0.37	0.74	1.04	0.98	2.02	1.31	11.39
MIN	0.25	0.01	0.08	0.05	0.03	0.01	0.00	0.00	0.00	0.00	0.09	0.07	5.89
YRS	9	10	9	10	9	9	10	10	10	10	10	9	6

Evaporation Data for Hermiston, OR													
Station	Year	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
35 3847 TEVP HI 1975		9999	9999	329B	521	834	964	1114	917	627	9999	9999	9999
35 3847 TEVP HI 1976		9999	9999	9999	488	823	939	1095	745	616	9999	9999	9999
35 3847 TEVP HI 1977		9999	9999	335	658	749	1033	1181	991	507	9999	9999	9999
35 3847 TEVP HI 1978		9999	9999	363B	401	803	1019	1127	918	561	9999	9999	9999
35 3847 TEVP HI 1979		9999	9999	457B	499	784	974	1191	947	638	9999	9999	9999
35 3847 TEVP HI 1980		9999	9999	395B	598	706	831	1088	964	655	9999	9999	9999
35 3847 TEVP HI 1981		9999	9999	355	572	807	882	1101	951	638B	9999	9999	9999
35 3847 TEVP HI 1982		9999	9999	364B	548	870	953	1177	1000	533	9999	9999	9999
35 3847 TEVP HI 1983		9999	9999	9999	9999	9999	9999	9999	9999	9999	9999	9999	9999
35 3847 TEVP HI 1984		9999	9999	9999	9999	9999	9999	9999	9999	9999	9999	9999	9999
35 3847 TEVP HI 1985		9999	9999	9999	9999	9999	9999	9999	9999	9999	9999	9999	9999
35 3847 TEVP HI 1986		9999	9999	9999	596	787	1096	1051	1034	569	9999	9999	9999
35 3847 TEVP HI 1987		9999	9999	344	592	796	955	1073	1041	756	9999	9999	9999
35 3847 TEVP HI 1988		9999	9999	9999	511	769	888	9999	9999	9999	9999	9999	9999
35 3847 TEVP HI 1989		9999	9999	9999	9999	784	9999	1222	1013	699	9999	9999	9999
35 3847 TEVP HI 1990		9999	9999	9999	636B	794	1055	1189	935	676	9999	9999	9999
35 3847 TEVP HI 1991		9999	9999	9999	9999	9999	9999	9999	9999	9999	9999	9999	9999
35 3847 TEVP HI 1992		9999	9999	9999	9999	9999	9999	9999	9999	9999	9999	9999	9999
Mean		0	0	3.67	5.517	7.93	9.657	11.34	9.546	6.229	0	0	0
SD dev				0.41	0.717	0.398	0.766	0.554	0.785	0.714			
max				4.57	6.58	8.70	10.96	12.22	10.41	7.56			
min				3.29	4.01	7.06	8.31	10.51	7.45	5.07			
years				8	12	13	12	12	12	12			